

## Integrated Kurtosis-Based Algorithm for Z-Notch Filter (I-kaz<sup>TM</sup>) Multilevel Coefficients Responses toward the Simultaneous Changes in Amplitude and Frequency of Signals

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**Abstract:** The response of Integrated Kurtosis-Based Algorithm for Z-Notch Filter (I-kaz<sup>TM</sup>) Multilevel coefficients toward the simultaneous changes in amplitude and frequency of signals was unknown. This study presents the coefficients responses toward the synthetic signals which vary in amplitude and frequency simultaneously. The I-kaz<sup>TM</sup> Multilevel coefficients, 3rd order (<sup>3</sup>Z<sup>∞</sup>), 4th order (<sup>4</sup>Z<sup>∞</sup>), 5th order (<sup>5</sup>Z<sup>∞</sup>), 6th order (<sup>6</sup>Z<sup>∞</sup>), 7th order (<sup>7</sup>Z<sup>∞</sup>) and 8th order (<sup>8</sup>Z<sup>∞</sup>) were investigated by analyzing their response using three types of synthetic signals, FIAI, FIAD and FDAI. The responses of the I-kaz<sup>TM</sup> Multilevel coefficients were analyzed by either increasing or decreasing the amplitude and frequency in the synthetic signals simultaneously. This study indicated that the response of all orders of I-kaz<sup>TM</sup> Multilevel coefficients showed an increasing trend with respect to the increment in amplitude of FIAI and FDAI. All the coefficients however showed a decreasing trend in FIAD synthetic signal study regardless the increase in the frequency. The study also indicated that the change in amplitude has more influence than the change in frequency in the I-kaz<sup>TM</sup> Multilevel coefficients responses. The influence ratio of the amplitude to frequency change was estimated to be 86.96-13.06%, respectively. Recognizing the behaviour of I-kaz<sup>TM</sup> Multilevel coefficients toward the change in amplitude and frequency is important especially when analysing dynamic signals.

**Key words:** Statistical analysis, digital signal processing, I-kaz<sup>TM</sup> method, digital signal filtering, signal decomposition, synthetic signal, fast Fourier transform

### INTRODUCTION

Statistical signal analysis is actually a mathematical science that involves data collection, analysis, interpretation and presentation (Nuawi *et al.*, 2008a). The main objective for the statistical analysis is to provide an easy and a simple analysis of a complex random signal.

Data at several levels could be revealed by the classification and interpretation of the signals (Chatfield and Collins, 1980). Common parameters such as the mean value, standard deviation value, the variance, the skewness, the kurtosis and the root mean square (rms) are used in statistical analysis (Pontuale *et al.*, 2003; Abdullah, 2005).

Average value, standard deviation, variance, skewness, kurtosis and root mean square (rms) are the common Signal Features (SFs) that can be used for extraction from any time domain signal (Sick, 2002; Ghosh *et al.*, 2007; Dong *et al.*, 2006). In order a signal to be able to adequately described and maintained the relevant information, SF from the captured signal need to

be properly derived (Teti *et al.*, 2010). Previous works related to I-kaz<sup>TM</sup> method were mainly on the application of this method on analyzing dynamic signals. The main objective of this study on the other hand, is to investigate the I-kaz<sup>TM</sup> Multilevel coefficients responses toward the simultaneous variation of amplitude and frequency in synthetic signals.

The mean value  $\bar{x}$  for a signal with n-number of data points is mathematically defined through Eq. 1, where  $x_i$  is the value of the data point. The mean value is one of the most important and often used parameters in indicating the tendency of the data toward the center:

$$\bar{x} = \frac{1}{n} \sum_{i=1}^n (x_i) \quad (1)$$

The standard deviation value is given by:

$$s = \left( \frac{1}{n} \sum_{i=1}^n (x_i - \bar{x})^2 \right)^{\frac{1}{2}} \quad (2)$$

where,  $x_i$  is the value of the data point and  $\bar{x}$  is the mean of the data. Base on Eq. 2, standard deviation value measures the spread of the data about the mean value. Variance is the square of the standard deviation as shown in Eq. 3:

$$\sigma = S^2 \tag{3}$$

Signal classification on the real-life signals base on mean and variance was not compatible mainly due to the signals contain outliers that can bring a noticeable shift in the actual value of both mean and variance (Pontuale *et al.*, 2003).

Skewness is the measurement of the asymmetry from the normal distribution in a set of statistical data. The skewness  $S$ , of a set of data is calculated base on the Eq. 4:

$$s = \frac{1}{nS^3} \sum_{i=1}^n (x_i - \bar{x})^3 \tag{4}$$

where,  $x_i$  is the value of the data point and  $\bar{x}$  is the mean of the data and  $s$  is the standard deviation value. Azrulhisham *et al.* (2012) in their study used skewness value to estimate the accelerated test model in fatigue life reliability evaluation of stub axle.

The signal 4th statistical moment Kurtosis  $K$ , is an important global signal statistic that is very sensitive to the spikiness of the data. The value of Kurtosis  $K$ , for discrete data sets is defined in Eq. 5:

$$K = \frac{1}{nS^4} \sum_{i=1}^n (x_i - \bar{x})^4 \tag{5}$$

The normal or Gaussian distribution, the Kurtosis value is approximately 3.0. The presence of more extreme value or amplitude than should be found in a Gaussian distribution can be detected when the kurtosis value is higher than 3.0.

In industries, statistical analysis using Kurtosis value were used frequently in detecting defect symptoms due to its sensitivity towards the existence of high amplitude (Pontuale *et al.*, 2003). A proper maintenance can be conducted systematically and accurately base on the measurement of Kurtosis value.

**Development of integrated kurtosis-based algorithm (I-kaz™):** I-kaz™ was formulated base on the concept of data distribution or scattering about its center points. It was developed with the purpose of giving descriptive and inferential statistics which is an advantage in comparison with other statistical methods that only rely on numerical

value. I-kaz™ coefficient,  $Z^3$  and the value was supported by a three dimensional graphical summarisations of frequency distribution (Nuawi *et al.*, 2008a).

In the original I-kaz™ coefficient calculation, a dynamic signal in time domain will be decomposed into three frequency band by following the 3rd order of the Daubechies concept in signal decomposition process (Daubechies, 1992). To calculate the sampling frequency of any signal in time domain, the Nyquist number must be 2 or greater than the maximum frequency in order to avoid the content of the sampling signal to be misinterpreted. Nyquist number in this calculation was chosen to be equal to 2 for the purpose of calculation simplification (Figliola and Beasley, 2000).

The sensitivity of the I-kaz™ coefficient toward amplitude and frequency change in a signal was proven far better than the current statistical parameters (Nuawi *et al.*, 2008a; Karim *et al.*, 2011). With this advantage, the I-kaz™ coefficient is very suitable in Signal Features (SF) translation. In previous researches, the structure-borne sound signal analyzed using I-kaz™ which correlated with the internal pipe surface condition showed a high ability to differentiate between the smooth and rough pipe surface (Nuawi *et al.*, 2009). Different study showed that the I-kaz™ method was capable of improving the Taylor curve which was unable to exhibit the three typical wear curve for the cutting that use certain cutting speed (Nuawi *et al.*, 2007). Ghani *et al.* (2011) in used the I-kaz™ coefficient to analyze the flank wear during turning process for tool wear prediction purpose.

**Development of I-kaz™ multilevel coefficient ( ${}^LZ^m$ ):** The development of I-kaz™ multilevel coefficient ( ${}^LZ^m$ ) was inspired by the original I-kaz™ ( $Z^m$ ) which was pioneered by Nuawi *et al.* (2008b). The new symbol for I-kaz™ Multilevel coefficient is defined as  ${}^LZ^m$  in which  $L$  is referring to the number of order of signal decomposition. The decomposition of signals in time domain into more frequency bands is to get a better coefficient response especially in the lower part of the frequency spectrum. The new developed coefficient ( ${}^LZ^m$ ) is expected to have more sensitivity towards amplitude and frequency change in a signal. In I-kaz™ Multilevel method, signal decomposition using  $L$ th order of Daubechies theorem will result in  $L$  number of frequency bands. This algorithm was summarized as presented in Fig. 1.

The frequency ranges of  $F_1, F_2, F_3$  to  $F_L$  in Fig. 1 are depending on the value of  $n$  and  $f_{max}$ . For I-kaz™Multilevel with  $L^{th}$  order of signal decomposition and for  $i = 1, 2, 3...L$ , the frequency ranges are shown below (Karim *et al.*, 2011):

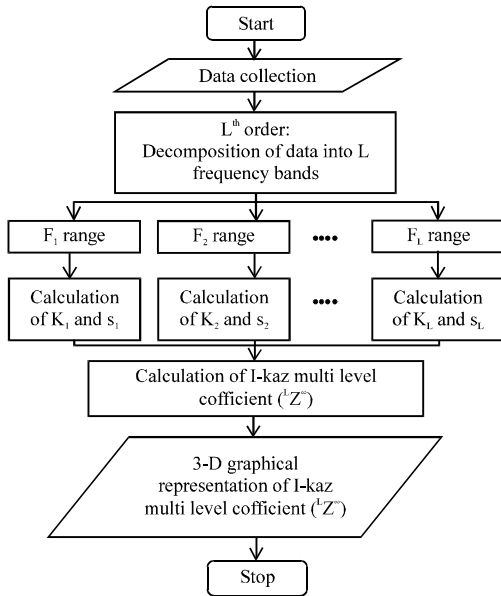


Fig. 1: Flowchart of the I-kaz™ Multilevel method

$$[F_{i=1 \min} = 0] \leq F_{i=1} \leq [F_{i=1 \max} = f_{\max}/(2^{L-1})] \quad (6)$$

$$[F_{i=2 \min} = F_{i=1 \max}] \leq F_{i=2} \leq [F_{i=2 \max} = f_{\max}/(2^{L-2})] \quad (7)$$

$$[F_{i=L \min} = F_{i=L-1 \max}] \leq F_{i=L} \leq [F_{i=L \max} = f_{\max}/(2^{L-L})] \quad (8)$$

The related I-kaz™ Multilevel coefficient can be calculated as (Karim *et al.*, 2011):

$${}^L Z^{\infty} = \frac{1}{n} \sqrt{K_1 S_1^4 + K_2 S_2^4 + K_3 S_3^4 \dots + K_L S_L^4} \quad (9)$$

where, L indicates the order of signal decomposition. Karim *et al.* (2012) in their study used the I-kaz™ Multilevel coefficient at level 7 of signal decomposition to correlate the wear rate of connecting rod bearing.

## MATERIALS AND METHODS

**Creating synthetic signals FIAI, FIAD and FDAI:** Three different synthetic signals, Frequency Increase and Amplitude Increase (FIAI), Frequency Increase and Amplitude Decrease (FIAD) and Frequency Decrease and Amplitude Increase (FDAI) were created with the same initial specifications. All signals were created by using MATLAB® and were defined with 512 data points and sampled at 1000 Hz ( $F_s = 1000$  Hz). The synthetic signals originally consist of 10, 25, 40, 55, 70, 100, 140, 200, 300 and 350 Hz sinusoidal waves. The plots of the signals in time and frequency domain are shown in Fig. 2a and b. The unit used in time domain for y axis is volt (V). The

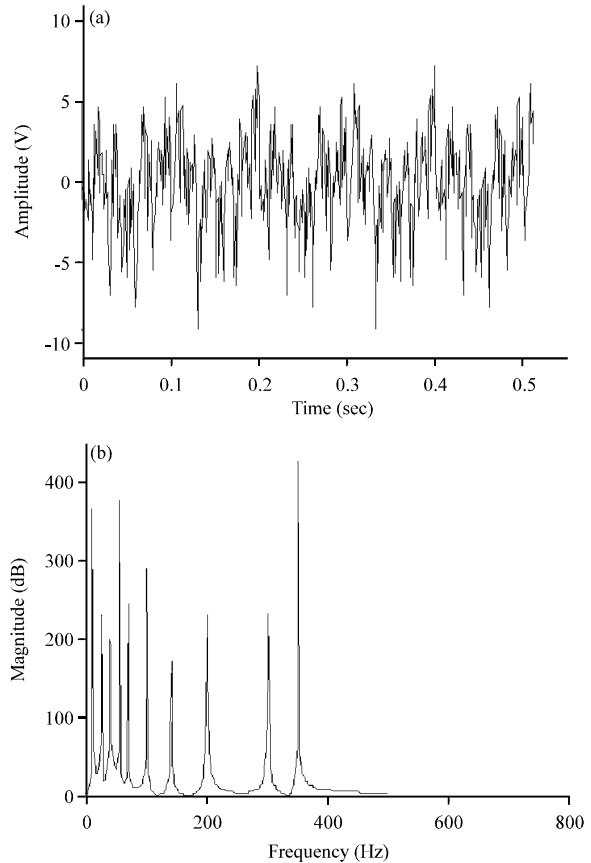


Fig. 2(a-b): (a) Time domain of the test signal and (b) Frequency domain of the test signal

Fast Fourier Transform (FFT) method was used to transform the signal in time domain to frequency domain (Nuawi *et al.*, 2008b).

The amplitude and frequency of the synthetic signals were increased by 10, 20, 30, 40% and 10, 20, 30 and 10 Hz, respectively. For each pair of incremental value, the higher order of I-kaz™ Multilevel coefficients were calculated and compared.

**Creating synthetic signals FRAI and FIAR:** Another two types of synthetic signals were created in order to identify the influence ratio of the amplitude and frequency in I-kaz™ Multilevel coefficient response. Frequency Remain and Amplitude Increase (FRAI) signal was used to investigate how much the I-kaz™ Multilevel coefficient response towards amplitude change. Whereas, Frequency Increase and Amplitude Remain (FIAR) signal was used to investigate how much the I-kaz™ Multilevel coefficient response towards frequency change. The initial specification of both FRAI and FIAR signals were the same as the specification in signal FIAI, FIAD and FDAI.

The amplitude of signal FRAI was increased by 40% while the frequencies were kept constant. For the amplitude increment, the higher order of I-kaz™ coefficients,  ${}^4Z^{\infty}$ ,  ${}^5Z^{\infty}$ ,  ${}^6Z^{\infty}$ ,  ${}^7Z^{\infty}$  and  ${}^8Z^{\infty}$  were calculated and compared.

In FIAR signal, the frequency was increased by the incremental of 40 Hz while the amplitude was kept constant. Similarly, for the frequency increment, the higher order of I-kaz™ coefficients,  ${}^4Z^{\infty}$ ,  ${}^5Z^{\infty}$ ,  ${}^6Z^{\infty}$ ,  ${}^7Z^{\infty}$  and  ${}^8Z^{\infty}$  were calculated and compared.

**RESULTS AND DISCUSSION**

The I-kaz™ method was applied in various field of study, such as automotive engine performance monitoring (Nuawi *et al.*, 2008b), fatigue analysis (Abdullah *et al.*, 2007; Putra *et al.*, 2010) and machining condition monitoring (Nuawi *et al.*, 2007; Jaharah *et al.*, 2009). Previous works related to I-kaz™ method were mainly on the application of this method on analyzing dynamic signals. There is no specific work on the investigation of the I-kaz™ Multilevel coefficients responses toward the simultaneous variation of amplitude and frequency in synthetic signals. The most related works related to this study is the study on the I-kaz™ Multilevel coefficient response toward the change in amplitude and frequency when one of them was increased and one of them was kept constant (Karim *et al.*, 2011; Nuawi *et al.*, 2008b). The results from these studies showed that the I-kaz™ Multilevel coefficient and the normal I-kaz™ coefficient response were mainly due the change in amplitude of signals. These results was in accordance with the result in this study.

**I-kaz™ multilevel coefficient response towards the FIAR signal:** Four types of signals from original FIAR signal were created by increasing its amplitude and frequency from 10-40% by 10% incremental. At the same time, the signal frequency is changed by 10-40 Hz by 10 Hz incremental. Figure 3a-b and 4a-b show the sample plot of FIAR signals in time and frequency domain after 20 and 40% amplitude increment and 20 and 40 Hz frequency increment, respectively.

The results of I-kaz™ ( $Z^{\infty}$ ) and I-kaz™ Multilevel coefficients ( ${}^LZ^{\infty}$ ) toward different level of amplitude and frequency for the FIAR signal are presented in Fig. 5 and Table 1.

The I-kaz™ Multilevel coefficient values increase linearly with the increase in amplitude and frequency of the FIAR signal. The superscript number on the top left of letter Z represents the level of signal decomposition. The sensitivity of all coefficients toward the amplitude change

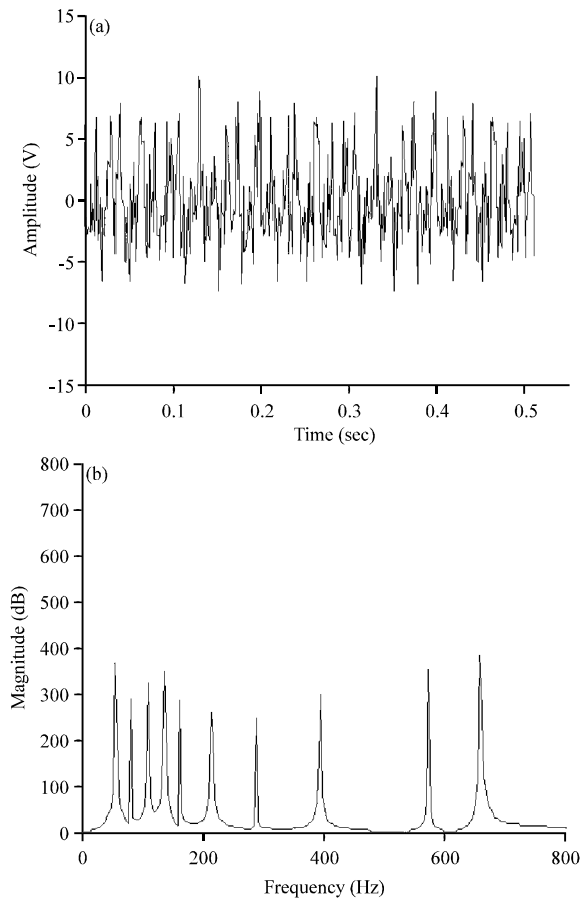


Fig. 3(a-b): The 20% Amplitude and 20 Hz frequency increase of FIAR signal (a) Time-domain (b) Frequency domain

Table 1: The respond of each coefficient in deviation percentage with respect to FIAR signal

Amplitude (%)	+10	+20	+30	+40
Frequency (Hz)	+10	+20	+30	+40
${}^3Z^{\infty}$	19.4969	44.0252	62.2642	81.1321
${}^4Z^{\infty}$	22.3140	44.6281	67.7686	96.6942
${}^5Z^{\infty}$	27.3585	57.5472	90.5660	123.5849
${}^6Z^{\infty}$	33.0000	67.0000	102.0000	137.0000
${}^7Z^{\infty}$	34.3434	68.6869	104.0404	139.3939
${}^8Z^{\infty}$	34.3434	68.6869	104.0404	139.3939

The coefficient symbol  ${}^3Z^{\infty}$ ,  ${}^4Z^{\infty}$ ,  ${}^5Z^{\infty}$ ,  ${}^6Z^{\infty}$ ,  ${}^7Z^{\infty}$  and  ${}^8Z^{\infty}$  represent the value of the coefficient calculated when the FIAR signal decomposed to 3, 4, 5, 6, 7 and 8 levels, respectively

can be seen clearly from Table 1. The higher the order of the I-kaz™ Multilevel coefficients, the more sensitive it responded to the amplitude and frequency change. For this type of particular synthetic signal, the sensitivity of the I-kaz™ Multilevel coefficient saturated at the 7th order ( ${}^7Z^{\infty}$ ).

**I-kaz™ multilevel coefficient response toward the FIAD signal:** Four types of signals from original FIAD signal

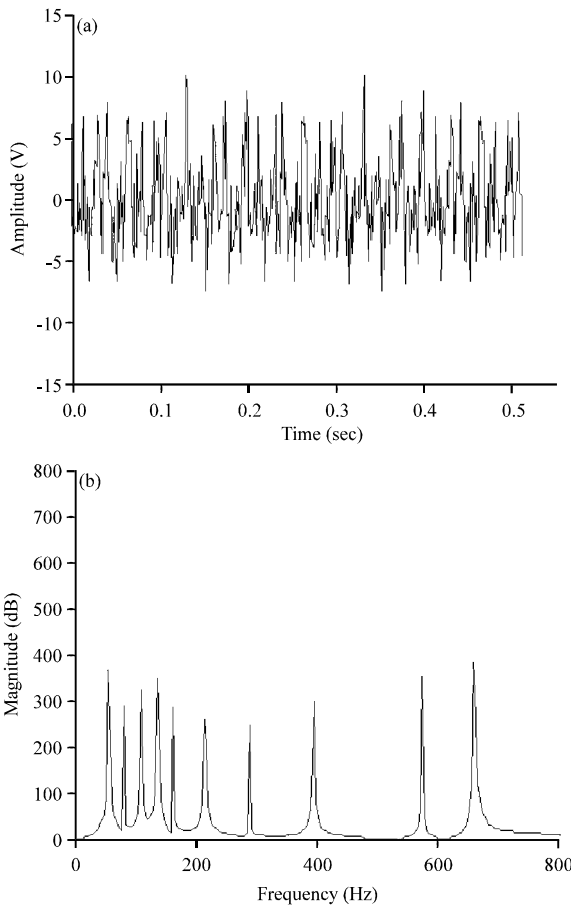


Fig. 4(a-b): The 40% Amplitude and 40 Hz frequency increase of FIAI signal (a) Time-domain (b) Frequency domain

were created by increasing its sinusoidal frequencies by 10 Hz incremental and decreasing its amplitude by 10% decremental as shown in Fig. 6a and b. Figure 7a and b show the sample plot of FIAD signal in time and frequency domain after 40 Hz frequency increment and 40% amplitude decrement of the FIAD.

The result of I-kaz<sup>TM</sup> ( $Z^m$ ) and I-kaz<sup>TM</sup> Multilevel coefficients ( ${}^1Z^m$ ) toward different degree of the FIAD signal are presented in Fig. 8 and Table 2.

The I-kaz<sup>TM</sup> Multilevel coefficient values decrease linearly when frequency is increased and amplitude is decreased. At this stage, the change in amplitude has more influence on the response of I-kaz<sup>TM</sup> Multilevel values. From Table 2, it was found that the most sensitive I-kaz<sup>TM</sup> Multilevel value was found at level 3.

**I-kaz<sup>TM</sup> multilevel coefficient response toward the FDAI signal:** Four types of signals from original FDAI signal were created by decreasing its sinusoidal frequencies by

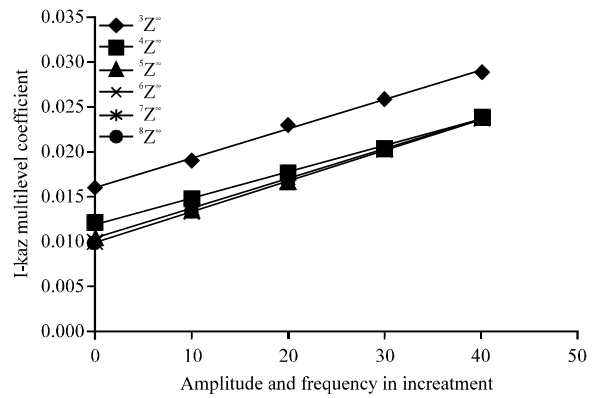


Fig. 5: The response of I-kaz<sup>TM</sup> Multilevel coefficient in FIAI signal

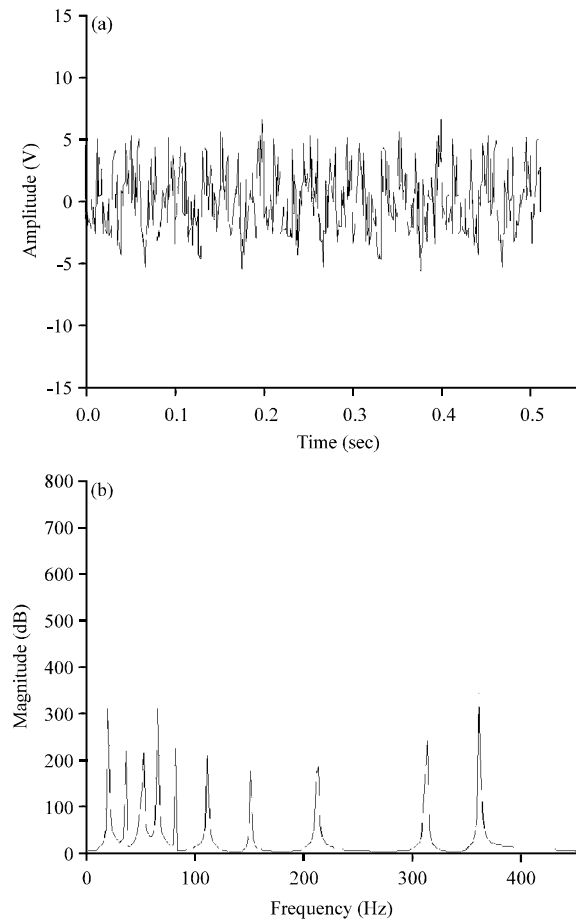


Fig. 6(a-b): The 10% amplitude decrease and 10 Hz frequency increase of FIAD signal (a) Time-domain (b) Frequency domain

10 Hz decremental and increasing its amplitude by 10% incremental. Figure 9a and b show the sample plot of FDAI signal in time and frequency domain after 10 Hz

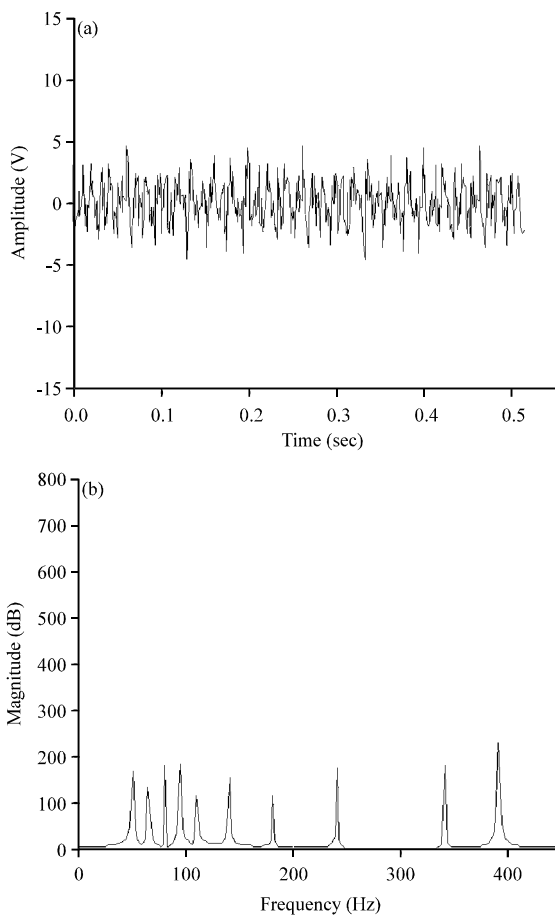


Fig. 7(a-b): The 40% amplitude decrease and 40 Hz frequency increase of FIAD signal  
(a) Time-domain (b) Frequency domain

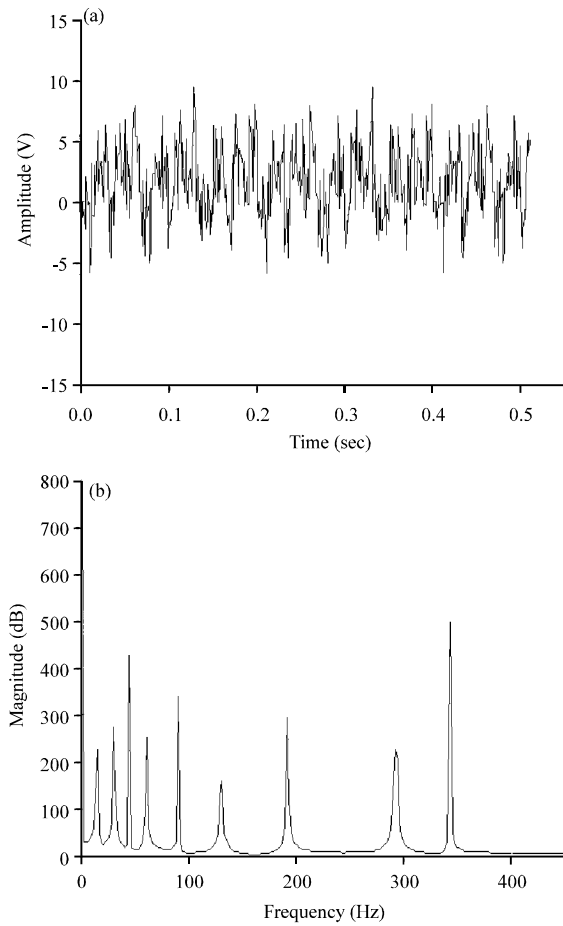


Fig. 9(a-b): The 10% amplitude increase and 10 Hz frequency decrease of FDAI signal  
(a) Time-domain (b) Frequency domain

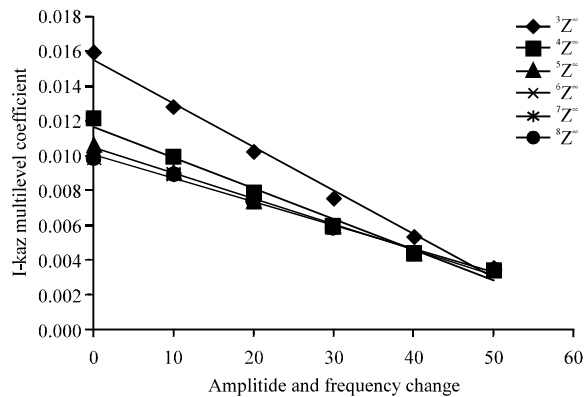


Fig. 8: The response of I-kaz™ Multilevel coefficient in FIAD signal

frequency increment and 10% amplitude reduction of FDAI signal. Figure 10a and b show the sample plot of

Table 2: The response of each coefficient in deviation percentage for FIAD signal

Amplitude (%)	-10	-20	-30	-40
Frequency (Hz)	+10	+20	+30	+40
${}^3Z^{\circ}$	-20.1258	-35.8491	-52.8302	-66.6667
${}^4Z^{\circ}$	-18.1818	-35.5372	-51.2397	-63.6364
${}^5Z^{\circ}$	-15.0943	-30.1887	-44.3396	-58.4906
${}^6Z^{\circ}$	-11.0000	-26.0000	-41.0000	-56.0000
${}^7Z^{\circ}$	-10.1010	-25.2525	-40.4040	-55.5556
${}^8Z^{\circ}$	-10.1010	-25.2525	-40.4040	-55.5556

${}^3Z^{\circ}$ ,  ${}^4Z^{\circ}$ ,  ${}^5Z^{\circ}$ ,  ${}^6Z^{\circ}$ ,  ${}^7Z^{\circ}$  and  ${}^8Z^{\circ}$ : Value of the coefficient calculated when the FIAD signal decomposed to 3, 4, 5, 6, 7 and 8 levels, respectively

FDAI signal in time and frequency domain after 40 Hz frequency increment and 40% amplitude reduction of FDAI signal.

The result of I-kaz™ ( $Z^{\circ}$ ) and I-kaz™ Multilevel coefficients ( ${}^LZ^{\circ}$ ) toward different degree of the FDAI signal are presented in Fig. 11 and Table 3.

The I-kaz™ Multilevel value increase linearly when the amplitude is increased and the frequency is decreased

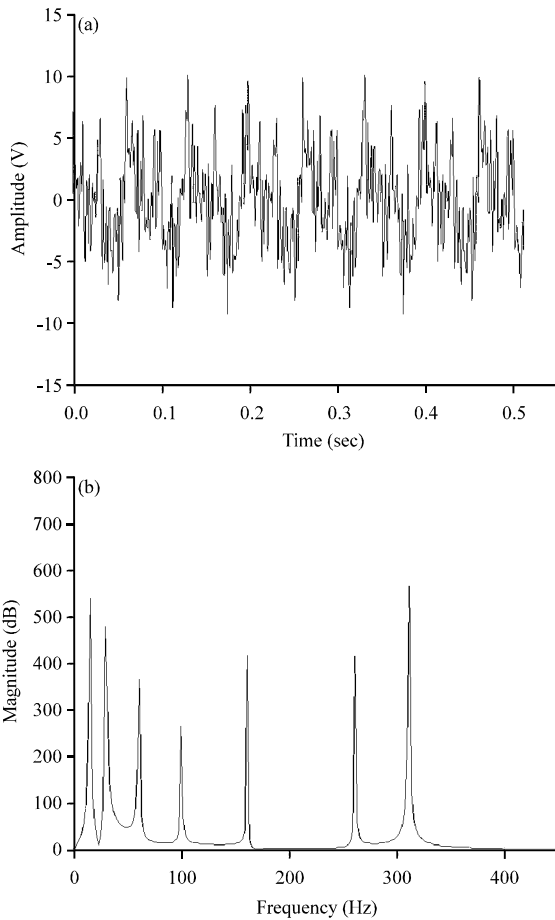


Fig. 10(a-b): The 40% amplitude increase and 40 Hz frequency decrease of FDAI signal  
(a) Time-domain (b) Frequency domain

Table 3: The response of each coefficient in deviation percentage for FDAI signal

Amplitude (%)	+10	+20	+30	+40
Frequency (Hz)	-10	-20	-30	-40
$^3Z^m$	22.5000	43.3333	58.3333	110.0000
$^4Z^m$	23.1579	50.5263	82.1053	126.3158
$^5Z^m$	21.4286	29.5918	48.9796	82.6531
$^6Z^m$	21.4286	26.5306	36.7347	57.1429
$^7Z^m$	21.4286	26.5306	36.7347	42.8571
$^8Z^m$	21.4286	26.5306	36.7347	39.7959

$^3Z^m$ ,  $^4Z^m$ ,  $^5Z^m$ ,  $^6Z^m$ ,  $^7Z^m$  and  $^8Z^m$ : Value of the coefficient calculated when the FDAI signal decomposed to 3, 4, 5, 6, 7 and 8 levels, respectively

in FDAI signal. The change of amplitude in FDAI signal has more influence in the I-kaz<sup>TM</sup> Multilevel value. The I-kaz<sup>TM</sup> Multilevel values are increasing following the increasing trend in amplitude even though the frequency is decreased. From Table 3, the most sensitive I-kaz<sup>TM</sup> Multilevel coefficient occur at level 3.

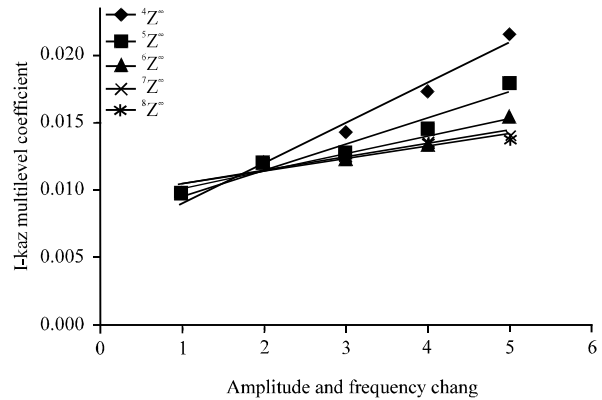


Fig. 11: The response of I-kaz<sup>TM</sup> multilevel coefficient in FDAI signal

Table 4: The Response of I-kaz<sup>TM</sup> Multilevel coefficients toward FIAR signal

Amplitude (%)	0	0	Difference (%)
Frequency (Hz)	0	+50	
$^3Z^m$	0.0159	0.0142	10.69
$^4Z^m$	0.0121	0.0134	10.74
$^5Z^m$	0.0106	0.0134	26.42
$^6Z^m$	0.0100	0.0134	34.00
$^7Z^m$	0.0099	0.0134	35.35
$^8Z^m$	0.0099	0.0134	35.35
Average	0.0114	0.0135	25.4263

$^3Z^m$ ,  $^4Z^m$ ,  $^5Z^m$ ,  $^6Z^m$ ,  $^7Z^m$  and  $^8Z^m$ : Value of the coefficient calculated when the FIAR signal decomposed to 3, 4, 5, 6, 7 and 8 levels, respectively

Table 5: The Response of I-kaz<sup>TM</sup> Multilevel coefficients toward FRAI signal

Amplitude (%)	0	+50	Difference (%)
Frequency (Hz)	0	0	
$^3Z^m$	0.0159	0.0358	125.16
$^4Z^m$	0.0121	0.0272	124.79
$^5Z^m$	0.0106	0.0238	124.53
$^6Z^m$	0.0100	0.0224	124.00
$^7Z^m$	0.0099	0.0223	125.25
$^8Z^m$	0.0099	0.0223	125.25
Average	0.0114	0.0256	124.83

$^3Z^m$ ,  $^4Z^m$ ,  $^5Z^m$ ,  $^6Z^m$ ,  $^7Z^m$  and  $^8Z^m$ : Value of the coefficient calculated when the FRAI signal decomposed to 3, 4, 5, 6, 7 and 8 levels, respectively

**I-kaz<sup>TM</sup> multilevel coefficient response toward the FRAI and FIAR signal:**

Synthetic signals FRAI and FIAR were created to investigate the percentage contribution of frequency and amplitude toward the change in I-kaz<sup>TM</sup> Multilevel coefficient value. Table 4 shows the value of I-kaz<sup>TM</sup> Multilevel coefficients calculated on FIAR signal when the frequency was increased to 50 Hz while the amplitude was kept constant. In Table 5, FRAI synthetic signals were used to calculate the value of I-kaz<sup>TM</sup> Multilevel coefficients in which the amplitude of this was increased to 50% while the frequency was kept constant.

The above results also clearly indicate that the amplitude change has more influence than the frequency change in FRAI and FIAR signals, respectively for the I-kaz<sup>TM</sup> Multilevel coefficient value. A very similar results

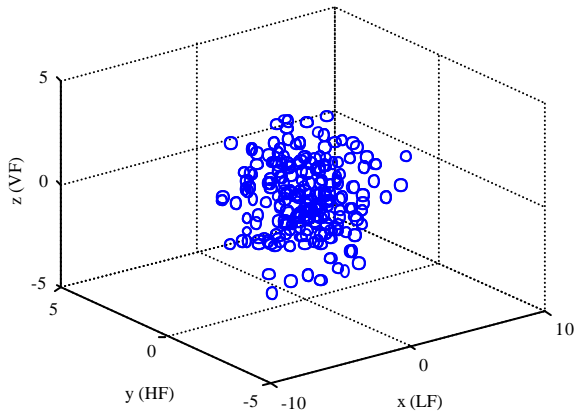


Fig. 12: FIAI original with calculated I-kaz multilevel coefficient ( ${}^7Z^{\circ}$ ) = 0.0099

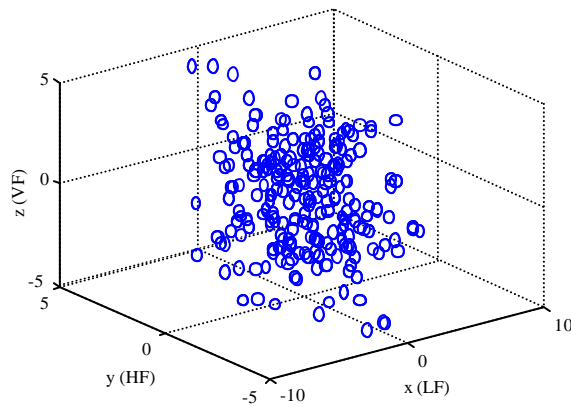


Fig. 13: FIAI after 40% and 40 Hz increased with calculated I-kaz multilevel coefficient ( ${}^7Z^{\circ}$ ) = 0.0023

were reported in the previous study by Karim *et al.* (2011) and Nuawi *et al.* (2008b) in their study to investigate the sensitivity of I-kaz<sup>TM</sup> coefficient versus the current statistical coefficient such as standard deviation, kurtosis, skewness and root mean square (rms).

The influence ratio of amplitude and frequency toward I-kaz<sup>TM</sup> Multilevel coefficient can be estimated by below equation:

$$\begin{aligned} \text{Amplitude influence} &= \frac{(\text{Avg I-kaz value FRAI@50}) - (\text{Avg I-kaz value FRAI@0})}{(\text{Avg I-kaz value FRAI@50}) + (\text{Avg I-kaz value FRAI@0})} \\ &= \frac{0.0256 - 0.0114}{0.0142 + 0.0021} \times 100 = 89.96\% \end{aligned}$$

$$\begin{aligned} \text{Frequency influence} &= \frac{(\text{Avg I-kaz value FRAI@50}) - (\text{Avg I-kaz value FRAI@0})}{(\text{Avg I-kaz value FRAI@50}) + (\text{Avg I-kaz value FRAI@0})} \\ &= \frac{0.0135 - 0.0114}{0.0142 + 0.0021} \times 100 = 13.04\% \end{aligned}$$

**I-kaz<sup>TM</sup> multilevel representation for FIAI signals:** The original I-kaz<sup>TM</sup> technique provide not only the coefficient value, but also a 3-D graphical illustration. The higher value of  ${}^LZ^{\circ}$  refers to the bigger space scattering of I-kaz<sup>TM</sup> Multilevel representation.

By using Eq. 6-8, for the Nyquist number equal to 2, frequency span equal to 1000 Hz,  $f_{\text{max}}$  equal to 500 Hz and L equal to 3, the frequency ranges of the I-kaz<sup>TM</sup> Multilevel representation can be summarized as follows:

- **x-axis:** Low Frequency (LF) range of 0-0.25  $f_{\text{max}}$
- **y-axis:** High Frequency (HF) range of 0.25  $f_{\text{max}}$ -0.5  $f_{\text{max}}$
- **z-axis:** Very high frequency (VF) range of 0.5  $f_{\text{max}}$ - $f_{\text{max}}$

The I-kaz<sup>TM</sup> Multilevel 3D representation and their coefficients values are shown in Fig. 12 and 13 for the original FIAI signal and the FIAI signal after 40% amplitude and 40 Hz 000011 frequency increase, respectively. The data distribution of the I-kaz<sup>TM</sup> Multilevel 3D representation for the Z-notch filtered signal in Fig. 13 was spread compared to the I-kaz<sup>TM</sup> Multilevel 3D representation in Fig. 12. Thus, the judgment of the existence of different signals can be based on the I-kaz<sup>TM</sup> Multilevel coefficient and also the I-kaz<sup>TM</sup> Multilevel 3D representation. A similar single I-kaz<sup>TM</sup> 3D scattering pattern was reported by Nuawi *et al.* (2008b) when studying for the filtered and the unfiltered signal in machining.

## CONCLUSION

This study discussed the response of I-kaz<sup>TM</sup> Multilevel coefficients toward the simultaneous change in amplitude and frequency of signals. This new I-kaz<sup>TM</sup> Multilevel method was proven to be very sensitive and detects very well in amplitude and frequency changes of measured signals.

In FIAI and FDAI signal study, all level of I-kaz<sup>TM</sup> Multilevel coefficients were noted to be increasing with the increase in amplitude regardless of the frequency condition, either increasing or decreasing. For both types of signals, the optimized value of I-kaz<sup>TM</sup> was found to be at the highest order of signal decomposition which is  ${}^8Z^{\circ}$ . The increasing rate of I-kaz<sup>TM</sup> Multilevel coefficients in response with FIAI signal is greater compare to the response in FDAI signal.

The study of FIAD showed that the I-kaz<sup>TM</sup> Multilevel coefficients were decreasing with the reduction in amplitude regardless of the increasing of the frequency in the signal. The optimized value of I-kaz<sup>TM</sup> Multilevel coefficient was found to be at the lowest order of signal decomposition which is  ${}^3Z^{\circ}$ .



In FIAI, FIAD and FDAI signal study, the response of I-kaz™ Multilevel coefficients are greatly depending on the amplitude change in the signals. The increasing or decreasing of the I-kaz™ Multilevel coefficients would follow the trend in the amplitude of the measured signals. The influence of amplitude and frequency in the I-kaz™ Multilevel coefficients response can be estimated in the FRAI and FIAR signals study. From this study, the influence ratio of amplitude and frequency is 86.96 and 13.04%, respectively. The study of this five different synthetic signals showed that the I-kaz™ Multilevel coefficients saturated at the highest level of signal decomposition except in the response of FIAD signal. Recognizing and understanding the behaviour of I-kaz™ Multilevel coefficients toward the change in amplitude and frequency is important especially when analysing dynamic signals.

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#### REFERENCES

- Abdullah, S., 2005. Wavelet Bump Extraction (WBE) for editing variable amplitude fatigue loadings. Ph.D. Thesis, University of Sheffield, United Kingdom.
- Abdullah, S., M.Z. Nuawi and A. Zaharim, 2007. Application of a computational data editing algorithm to summarise fatigue road loadings. WSEAS Tran. Comput. Res., 2: 109-114.
- Azrulhisham, E.A., Y.M. Asri, A.W. Dzuraidah and A.H. Hairul Fahmi, 2012. Accelerated Test Model in Fatigue Life Reliability Evaluation of Stub Axle. In: Advances in Safety, Reliability and Risk Management, Berenguer, C., A. Grall and C.G. Soares (Eds.). Taylor and Francis Group, London, ISBN: 9780415683791, Pages: 3076.
- Chatfield, C. and A.J. Collins, 1980. An Introduction to Multi Vibrate Analysis. Chapman and Hall, London.
- Daubechies, I., 1992. Ten Lectures on Wavelets. SIAM, Philadelphia, USA.
- Dong, J., K.V.R. Subrahmanyam, Y.S. Wong, G.S. Hong and A.R. Mohanty, 2006. Bayesian inference-based neural networks for tool wear estimation. Int. J. Adv. Manuf. Technol., 30: 797-807.
- Figliola, R.S. and D.E. Beasley, 2000. Theory and Design for Mechanical Measurements. 3rd Edn., John Wiley and Sons, Hoboken, USA.
- Ghani, J.A., M. Rizal, M.Z. Nuawi, M.J. Ghazali and C.H.C. Haron, 2011. Monitoring online cutting tool wear using low-cost technique and user friendly GUI. Wear, 271: 2619-2624.
- Ghosh, N., Y.B. Ravi, A. Patra, S. Mukhopadhyay, S. Paul, A.R. Mohanty and A.B. Chattopadhyay, 2007. Estimation of tool wear during CNC milling using neural network-based sensor fusion. Mech. Syst. Signal Process., 21: 466-479.
- Jaharah, A.G., C.H. Che Hassan, M.J. Ghazali, A.B. Sulong, M.Z. Omar, M.Z. Nuawi and A.R. Ismail, 2009. Performance of uncoated carbide cutting tool when machining cast iron in dry cutting condition. Int. J. Mod. Phys. B, 23: 1796-1802.
- Karim, Z., M.Z. Nuawi, J.A. Ghani, S. Abdullah and M.J. Ghazali, 2011. Optimization of integrated kurtosis-based algorithm for z-notch filter (I-Kaz™) coefficient using multi level signal decomposition technique. World Applied Sci. J., 14: 1541-1548.
- Karim, Z., M.Z. Nuawi, J.A. Ghani, S. Abdullah and M.J. Ghazali, 2012. Wear monitoring of connecting rod bearing via air-borne method analyzed by using I-kaz™ multi level value. Adv. Mater. Res., 445: 941-946.
- Nuawi, M. Z., F. Lamin, M.J.M. Nor, N. Jamaluddin, S. Abdullah and C.K.E. Nizwan, 2007. Integration of I-kaz coefficient and Taylor tool life curve for tool wear progression monitoring in machining process. Int. J. Mechanics, 4: 44-50.
- Nuawi, M.Z., M.J.M. Nor, N. Jamaludin, S. Abdullah, F. Lamin and C.K.E. Nizwan, 2008a. Development of integrated kurtosis-based algorithm for z-filter technique. J. Applied Sci., 8: 1541-1547.
- Nuawi, M.Z., S. Abdullah, A.R. Ismail, R. Zulkifli, M.K. Zakaria and M.F.H. Hussin, 2008b. A study on ultrasonic signals processing generated from automobile engine block using statistical analysis. WSEAS Trans. Signal Proc., 4: 279-288.
- Nuawi, M.Z., S. Abdullah, F. Lamin, A.R. Ismail and M.J.M. Nor, 2009. Correlation of structure-borne sound signal and internal piping surface condition using integrated kurtosis-based algorithm for Z-notch filter technique (I-kaz). Proceedings of the 16th International Congress on Sound and Vibration, July 5-9, 2009, Krakow, Poland.

- Pontuale, G., F.A. Farelly, A. Petri and L. Pitolli, 2003. A statistical analysis of acoustic emission signals for tool condition monitoring (TCM). *Acoustics Rev. Lett. Online*, 4: 13-18.
- Putra, T.E., S. Abdullah, M.Z. Nuawi and Z.M. Nopiah, 2010. Wavelet coefficient extraction algorithm for extracting fatigue features in variable amplitude fatigue loading. *J. Applied Sci.*, 10: 277-283.
- Sick, B., 2002. On-line and indirect tool wear monitoring in turning with artificial neural networks: A review of more than a decade of research. *Mech. Syst. Signal Process.*, 16: 487-546.
- Teti, R., K. Jemielniak, G. O'Donnell and D. Dornfeld, 2010. Advanced monitoring of machining operations. *CIRP Ann. Manuf. Technol.*, 59: 717-739.