



UNIVERSITI KUALA LUMPUR  
MALAYSIAN INSTITUTE OF CHEMICAL AND BIO-ENGINEERING TECHNOLOGY

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**FINAL EXAMINATION**  
**OCTOBER 2025 SEMESTER**

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COURSE CODE : CPD22203  
COURSE TITLE : MASS TRANSFER  
PROGRAMME NAME : DIPLOMA IN CHEMICAL ENGINEERING TECHNOLOGY  
DATE : 26 JANUARY 2026  
TIME : 9:00AM - 12:00PM  
DURATION : 3 HOURS

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**INSTRUCTIONS TO CANDIDATES**

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1. Please read the instructions given in the question paper CAREFULLY.
2. This question paper is printed on both sides of the paper.
3. This question paper consist of TWO sections.
4. Section A consist total of 60 marks. Answer ALL questions.
5. Section B consist of three questions. Answer TWO (2) questions only.
6. Please write your answer on the answer booklet provided.
7. Please answer all questions in English only.
8. Refer to the attached Formula/ Appendies. ☐ *Tick if applicable*

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THERE ARE 11 PAGES OF QUESTIONS INCLUDING THIS PAGE

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## SECTION A (Total: 60 marks)

Answer ALL questions.

Please use the answer booklet provided.

## Question 1

Answer the following Questions.

All separation processes are based on the principle of mass transfer and diffusion.

- (a) Explain the significance of the negative sign in Fick's First Law equation.  
(2 marks)
- (b) List FOUR(4) key factors affecting diffusion process.  
(4 marks)
- (c) Describe how a decrease in temperature affects the rate of diffusion in a system.  
(2 marks)
- (d) Identify one characteristic of equimolar counter diffusion in a binary gas system.  
(2 marks)
- (e) A binary gas mixture consisting of gases A and B undergoes equimolar counter diffusion in a stationary tube of length 1.0 m. Both ends of the tube are connected to large chambers, so the gas compositions at the ends remain constant. The mole fraction of gas A at point 1 is 0.8, while at point 2 it is 0.2. The total molar concentration of the gas mixture is  $4 \text{ mol/m}^3$ . The diffusivity of gas A in gas B is  $2.5 \times 10^{-5} \text{ m}^2/\text{s}$ . Estimate the diffusion flux of component A,  $J_A$ , in  $\text{mol/m}^2\cdot\text{s}$ .  
(5 marks)

**Question 2**

Answer the following questions

- (a) Define the reflux in a distillation column.  
(2 marks)
- (b) Differentiate between total reflux and minimum reflux ratio in a distillation column.  
(4 marks)
- (c) Explain the effect of the number of trays or stages on distillation column efficiency.  
(2 marks)
- (d) State TWO differences between bubble cap tray and sieve tray used in a distillation column.  
(2 marks)
- (e) Estimate the compositions of vapour ( $y_A$ ) and liquid ( $x_A$ ) for Benzene (A) in equilibrium with toluene (B) at temperature  $95^\circ\text{C}$  and total pressure of  $101.32\text{ kPa}$ . Given the vapor pressure of Benzene and Toluene are  $1168\text{ mmHg}$  and  $475\text{ mmHg}$ , respectively.  
(5 marks)

**Question 3**

Answer the following question.

- (a) List TWO(2) important properties of a good solvent used in gas absorption processes.

(2 marks)

- (b) Explain the types of liquid solvent that can affect the efficiency of gas absorption process in industry.

(2 marks)

- (c) Describe the application of Henry's Law to estimate the amount of gas absorbed in a solvent for gas absorption process.

(2 marks)

- (d) Describe a packed absorption tower process based on vapor-liquid contact type and pressure drop.

(4 marks)

- (e) At 303 K, hydrogen sulfide ( $\text{H}_2\text{S}$ ) is dissolved in water in a gas absorption system. The amount of  $\text{H}_2\text{S}$  in water is  $2.65 \times 10^{-6}$  kmol, and the amount of water is 0.0555 kmol. The Henry's Law constant(H) for  $\text{H}_2\text{S}$ –water at 303 K is  $0.0609 \times 10^4$  atm/mole fraction. Estimate the partial pressure of  $\text{H}_2\text{S}$  in the gas phase that must be maintained to prevent  $\text{H}_2\text{S}$  from escaping the aqueous solution.

(5 marks)

**Question 4**

Answer the following question.

- (a) Define the distribution coefficient( $K$ ) in liquid-liquid extraction.  
(2 marks)
- (b) Differentiate between the extract and raffinate phases in terms of solute concentration.  
(2 marks)
- (c) Describe the effect of temperature on the efficiency of solid-liquid extraction.  
(2 marks)
- (d) Discuss the effect of agitation on solid-liquid extraction.  
(2 marks)
- (e) Identify the correct composition of a mixture on a triangular diagram based on given Figure.

*Refer Below - Figure1 : Right Triangular Diagram of LLE .*

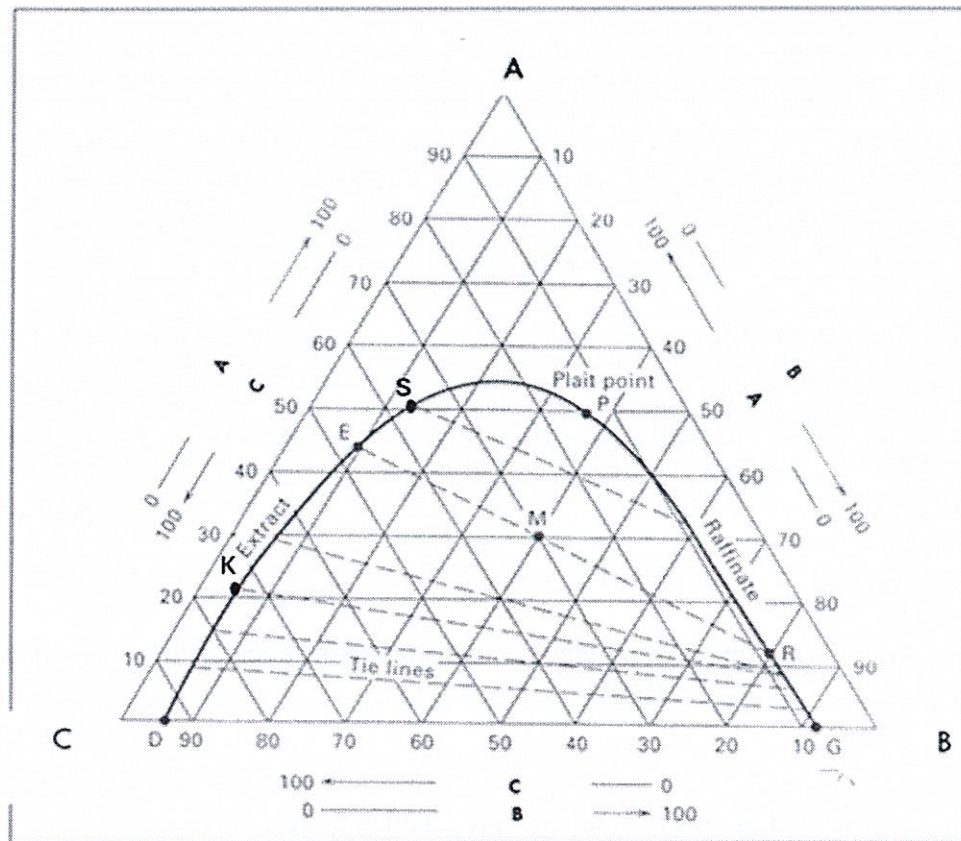


Figure 1: Right Triangular Diagram of LLE

i. Point K

(1 marks)

ii. Point S

(1 marks)

- (f) 200 kg of aqueous solution containing 50 wt% acetone is contacted with 600 kg of pure chlorobenzene, followed by separation of the extract and the raffinate phase. The solvent composition at mixing point (M) is  $x_{CM} = 0.725$ . It has been found from graphical method that the composition obtained for extract layer,  $V_1$  is  $y_{A1} = 0.08$  and  $y_{C1} = 0.9$ , Raffinate layer,  $L_N$  is  $x_{AN} = 0.04$  and  $x_{CN} = 0.017$ . Estimate the amount of extract ( $V_1$ ) and raffinate phases  $L_N$ .

(5 marks)

## SECTION B (Total: 40 marks)

Answer TWO (2) questions only.

Please use the answer booklet provided.

## Question 1

Answer the following question.

A continuous fractionating column is to be designed to separate a benzene-toluene mixture, with a feed rate of 14,000 kg/hr. The mixture consists of 56 mol% toluene and 44 mol% benzene. The goal is to produce a distillate product containing 97 mol% benzene and a bottom product containing 98 mol% toluene, under a pressure of 1 atm (101.3 kPa). The feed is preheated and enters the column as a partially vaporized mixture, with 60% in the vapor phase and the remaining 40% in the liquid phase. The equilibrium data for benzene are provided in the table below.

*Refer Below - Table1 : Vapor - liquid Equilibrium data for Component Benzene .*

Table 1: Vapor - liquid Equilibrium data for Component Benzene

|   |   |      |      |      |      |      |      |      |      |      |     |
|---|---|------|------|------|------|------|------|------|------|------|-----|
| x | 0 | 0.1  | 0.2  | 0.3  | 0.4  | 0.5  | 0.6  | 0.7  | 0.8  | 0.9  | 1.0 |
| y | 0 | 0.22 | 0.39 | 0.52 | 0.63 | 0.71 | 0.79 | 0.85 | 0.91 | 0.96 | 1.0 |

- (a) Estimate the minimum reflux ratio ( $R_{\min}$ ) for this separation. (8 marks)
- (b) Determine number of theoretical stages required using McCabe-Thiele method, if reflux ratio of three times the reflux minimum is used as obtained in answer (a). (8 marks)
- (c) Explain how increasing the reflux ratio affects the number of theoretical stages required and the operating lines in the McCabe-Thiele diagram for a distillation column. (4 marks)

**Question 2**

Answer the following question.

100 kg of granulated halibut livers are extracted to produce 26 wt% of oil in a countercurrent multi-batch arrangement by using 50 kg of ether as solvent. It is desired to obtain 80% of oil recovery in the overflow product. The total solution containing solute and solvent in the overflow product is 47.27 kg. It has been found experimentally that the amount of the solution removed in the underflow in association with every kilogram of insoluble matter is given by table below.

*Refer Below - Table2 : The entrainment data of oil solute in overflow .*

Table 2: The entrainment data of oil solute in overflow

| Mass fraction of solute(oil)<br>(overflow),<br><br>$y_A$ | Entrainment<br>(kg solution/kg Inert)<br><br>$k$ |
|----------------------------------------------------------|--------------------------------------------------|
| 0                                                        | 0.28                                             |
| 0.1                                                      | 0.30                                             |
| 0.2                                                      | 0.40                                             |
| 0.3                                                      | 0.47                                             |
| 0.4                                                      | 0.55                                             |
| 0.5                                                      | 0.66                                             |
| 0.6                                                      | 0.8                                              |
| 0.67                                                     | 0.96                                             |

- (a) Produce the underflow data in term of mass fraction for oil solute ( $x_A$ ) and solvent( $x_S$ ).  
(5 marks)
- (b) Calculate the composition for underflow outlet product for solute ( $x_{A_{N+1}}$ ) and solvent( $x_{S_{N+1}}$ ).  
(7 marks)

- (c) Calculate the number of stages required for this extraction using right angle triangular diagram.

(8 marks)

**Question 3**

Answer the following question.

Pure solvent at the rate of 580 kg/h is being used to extract an aqueous solution of 220 kg/h containing 35 wt% solute by counter-current multistage extraction. The desired exit solute in the aqueous phase is 5wt%. It has been found the composition of mixing point(M) is  $x_{CM} = 0.725$  and  $x_{AM} = 0.096$ . The table below presents the liquid-liquid equilibrium data for this system.

*Refer Below - Table3 : Liquid-Liquid Solubility Equilibrium Data .*

Table 3: Liquid-Liquid Solubility Equilibrium Data

| Raffinate Layer |          |         | Extract Layer |          |         |
|-----------------|----------|---------|---------------|----------|---------|
| Solute          | Solution | Solvent | Solute        | Solution | Solvent |
| 0               | 0.988    | 0.012   | 0             | 0.006    | 0.994   |
| 0.029           | 0.955    | 0.016   | 0.008         | 0.008    | 0.984   |
| 0.133           | 0.844    | 0.023   | 0.048         | 0.019    | 0.933   |
| 0.369           | 0.589    | 0.044   | 0.216         | 0.069    | 0.715   |
| 0.464           | 0.371    | 0.165   | 0.362         | 0.151    | 0.487   |

- (a) Construct the Right-Angle Triangular diagram Graph (Mass fraction Solvent, ( $x_c, y_c$ ) against mole fraction Solute ( $x_A, y_A$ )) in extract and raffinate phase for this extraction process.  
(7 marks)
- (b) Estimate the outlet composition of the extract  $V_1$  and the aqueous raffinate  $L_1$  from the answer(a).  
(8 marks)
- (c) Find the number of stages for this separation.  
(5 marks)

END OF EXAMINATION PAPER

## Appendix A

$$R = 8.314 \frac{\text{m}^3 \cdot \text{kPa}}{\text{kgmol} \cdot \text{K}}$$

$$J_A = -D_{AB} \frac{dc_A}{dz}$$

$$J_A = -\frac{cD_{AB}}{(z_2 - z_1)} (y_{A2} - y_{A1})$$

$$J_A = \frac{D_{AB}(p_{A1} - p_{A2})}{RT(z_2 - z_1)}$$

$$p_A + p_B = P$$

$$p_i = P_i x_i$$

$$P_A x_A + P_B (1 - x_A) = P$$

$$y_i = \frac{P_i x_i}{P}$$

$$y_A = \frac{\alpha_{AB} x_A}{1 + (\alpha_{AB} - 1)x_A}$$

$$y_{n+1} = \frac{R}{R+1} x_n + \frac{1}{R+1} x_D$$

$$y_q = \frac{q}{q-1} x_q - \frac{x_F}{q-1}$$

$$y^* = \frac{R_{\min}}{R_{\min} + 1} x^* + \frac{1}{R_{\min} + 1} x_D$$

$$R_{\min} = \frac{x_D - y^*}{y^* - x^*}$$

$$L\left(\frac{x_2}{1-x_2}\right) + V'\left(\frac{y_1}{1-y_1}\right) = L\left(\frac{x_1}{1-x_1}\right) + V'\left(\frac{y_2}{1-y_2}\right)$$

$$L\left(\frac{x_0}{1-x_0}\right) + V'\left(\frac{y_{N+1}}{1-y_{N+1}}\right) = L\left(\frac{x_N}{1-x_N}\right) + V'\left(\frac{y_1}{1-y_1}\right)$$

$$y_{n+1} = \frac{L_n x_n}{V_{n+1}} + \frac{V_1 y_1 - L_0 x_0}{V_{n+1}}$$

$$x_A = \frac{y_A k}{1+k}$$

$$x_S = \frac{k(1-y_A)}{1+k}$$

$$x_B = \frac{1}{K+1}$$

$$x_{CM} = \frac{Fx_{FC} + Sy_{SC}}{F + S}$$

$$x_{AM} = \frac{Fx_{FA} + Sy_{SA}}{F + S}$$

$$L_0 + V_{N+1} = L_N + V_1 = M$$

$$L_0 x_{C0} + V_{N+1} y_{N+1} = L_N x_{CN} + V_1 y_{C1} = M x_{CM}$$

$$x_{CM} = \frac{L_0 x_{C0} + V_{N+1} y_{CN+1}}{L_0 + V_{N+1}} = \frac{L_N x_{CN} + V_1 y_{C1}}{L_N + V_1}$$

$$x_{AM} = \frac{L_0 x_{A0} + V_{N+1} y_{AN+1}}{L_0 + V_{N+1}} = \frac{L_N x_{AN} + V_1 y_{A1}}{L_N + V_1}$$

$$\text{mole} = \frac{\text{mass}}{\text{molecular weight}}$$

$$\text{average MW (in term of mass fraction)} \frac{1}{\bar{M}} = \sum \frac{x_i}{M_i}$$

$$\text{average MW (in term of mole fraction), } \bar{M} = \sum y_i M_i$$

$$\text{Molar flowrate} = \frac{\text{mass flowrate}}{\text{molecular weight}}$$

$$\text{Mole fraction, } y_A = \frac{\text{mole of A}}{\text{total mole}}$$

$$\text{Mass fraction, } x_A = \frac{\text{Mass of A}}{\text{total mass}}$$

## FACTORS FOR UNIT CONVERSIONS

| Quantity           | Equivalent Values                                                                                                                                                                                                                                                                                                                                                                                                                            |
|--------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>Mass</b>        | $1 \text{ kg} = 1000 \text{ g} = 0.001 \text{ metric ton} = 2.20462 \text{ lb}_m = 35.27392 \text{ oz}$<br>$1 \text{ lb}_m = 16 \text{ oz} = 5 \times 10^{-4} \text{ ton} = 453.593 \text{ g} = 0.453593 \text{ kg}$                                                                                                                                                                                                                         |
| <b>Length</b>      | $1 \text{ m} = 100 \text{ cm} = 1000 \text{ mm} = 10^6 \text{ microns } (\mu\text{m}) = 10^{10} \text{ angstroms } (\text{\AA})$<br>$= 39.37 \text{ in} = 3.2808 \text{ ft} = 1.0936 \text{ yd} = 0.0006214 \text{ mile}$<br>$1 \text{ ft} = 12 \text{ in} = 1/3 \text{ yd} = 0.3048 \text{ m} = 30.48 \text{ cm}$                                                                                                                           |
| <b>Volume</b>      | $1 \text{ m}^3 = 1000 \text{ liters} = 10^6 \text{ cm}^3 = 10^6 \text{ ml}$<br>$= 35.3145 \text{ ft}^3 = 220.83 \text{ imperial gallons} = 264.17 \text{ gal}$<br>$= 1056.68 \text{ qt}$<br>$1 \text{ ft}^3 = 1728 \text{ in}^3 = 7.4805 \text{ gal} = 0.028317 \text{ m}^3 = 28.317 \text{ liters}$<br>$= 28\,317 \text{ cm}^3$                                                                                                             |
| <b>Force</b>       | $1 \text{ N} = 1 \text{ kg}\cdot\text{m}/\text{s}^2 = 10^5 \text{ dynes} = 10^5 \text{ g}\cdot\text{cm}/\text{s}^2 = 0.22481 \text{ lb}_f$<br>$1 \text{ lb}_f = 32.174 \text{ lb}_m\cdot\text{ft}/\text{s}^2 = 4.4482 \text{ N} = 4.4482 \times 10^5 \text{ dynes}$                                                                                                                                                                          |
| <b>Pressure</b>    | $1 \text{ atm} = 1.01325 \times 10^5 \text{ N}/\text{m}^2 (\text{Pa}) = 101.325 \text{ kPa} = 1.01325 \text{ bars}$<br>$= 1.01325 \times 10^6 \text{ dynes}/\text{cm}^2$<br>$= 760 \text{ mm Hg at } 0^\circ\text{C} (\text{torr}) = 10.333 \text{ m H}_2\text{O at } 4^\circ\text{C}$<br>$= 14.696 \text{ lb}_f/\text{in}^2 (\text{psi}) = 33.9 \text{ ft H}_2\text{O at } 4^\circ\text{C}$<br>$= 29.921 \text{ in Hg at } 0^\circ\text{C}$ |
| <b>Energy</b>      | $1 \text{ J} = 1 \text{ N}\cdot\text{m} = 10^7 \text{ ergs} = 10^7 \text{ dyne}\cdot\text{cm}$<br>$= 2.778 \times 10^{-7} \text{ kW}\cdot\text{h} = 0.23901 \text{ cal}$<br>$= 0.7376 \text{ ft}\cdot\text{lb}_f = 9.486 \times 10^{-4} \text{ Btu}$                                                                                                                                                                                         |
| <b>Power</b>       | $1 \text{ W} = 1 \text{ J}/\text{s} = 0.23901 \text{ cal}/\text{s} = 0.7376 \text{ ft}\cdot\text{lb}_f/\text{s} = 9.486 \times 10^{-4} \text{ Btu}/\text{s}$<br>$= 1.341 \times 10^{-3} \text{ hp}$                                                                                                                                                                                                                                          |
| <b>Temperature</b> | $T(\text{K}) = T(^{\circ}\text{C}) + 273.15$<br>$T(^{\circ}\text{F}) = 1.8 T(^{\circ}\text{C}) + 32$<br>$T(^{\circ}\text{R}) = T(^{\circ}\text{F}) + 459.67$<br>$T(^{\circ}\text{R}) = 1.8 T(\text{K})$                                                                                                                                                                                                                                      |

