



UNIVERSITI KUALA LUMPUR
MALAYSIA FRANCE INSTITUTE

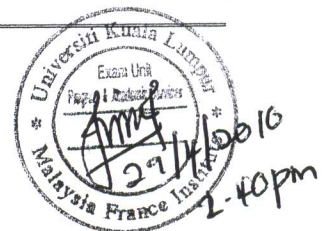
FINAL EXAMINATION
JANUARY 2010 SESSION

SUBJECT CODE : FRB40103
SUBJECT TITLE : TECHNOLOGY OF INDUSTRIAL REFRIGERATION
LEVEL : BACHELOR
TIME/DURATION : 9.00 am – 1:00 pm
4 HOURS
DATE : 5 May 2010

INSTRUCTIONS TO CANDIDATES

1. All documents authorized (Open Book Examination)
 2. Please read the instructions given in the question paper CAREFULLY.
 3. This question paper is printed on both sides of the paper.
 4. Please write your answers on the answer booklet provided.
 5. Answer should be written in blue or black ink except for sketching, graphic and illustration.
 6. This question paper consists only one section. Answer all questions.
 7. Answer all questions in English.
-

THERE ARE 10 PRINTED PAGES OF QUESTIONS.



INSTRUCTION: Answer ALL questions.

Please use the answer booklet provided.

PART A

A factory daily receive 100 000 litres of milk in the morning (08 00) and 100 000 litres of milk in the evening (20 00). Milk is received with 6°C and need to be cooled to 4°C in 2 hours.

Question 1

a) Calculate the required refrigerating power for this cooling.

[Take CP of milk as 4.18kJ / kg. K]

(1 marks)

b) Calculate the cooling energy.

(0.5 marks)

Milk is then processed using the following equipment:

| | Power (kW) | Schedules of operation | |
|-------------------|------------|------------------------|-------|
| | | ON | OFF |
| Separator | 120 | 10h00 | 14h00 |
| Pasteurizer | 250 | 10h00 | 14h00 |
| Maturator | 50 | 12h00 | 16h00 |
| Tunnel of cooling | 300 | 14h00 | 18h00 |
| Cold room | 80 | 0h00 | 24h00 |

Table 1.1 Schedule of operation of equipment

c) To establish the histogram of the needs for the factory (in the form of table only)

(1 marks)

For this application, a designer proposes to install a refrigerating power of 920kW

d) What do you think about this choice? What power would you propose to install? (Justify your choice by the concept of thermal energy storage)

(0.5 marks)

Question 2

What advice would you give to your client regarding the operation time of the refrigeration system, without modifying the schedule of operation of varies equipment stated in the table 1.1 above.

(Note: Your objective is to limit the maximum demand of electricity consumption)

(1 marks)

Question 3

Between a solution of direct expansion and a system with secondary fluid and between a halogenous refrigerant (HCFC, HFC) and ammonia, what solution proposes to be adopted? (Justify your choice by having the advantages and disadvantages of each solution).

(2 marks)

PART B

The solution finally retained is to install a capacity of 800 kW by using an installation of ammonia produce glycol water at -8°C by 2 flood plate exchangers supplied by LP bottle. The cycle is single stage operate in a mode $-12^{\circ}\text{C} / +35^{\circ}\text{C}$ with screw compressors, each with its own oil-separator. The condenser is common to the compressors. The cooling of oil is carried out by water cooled exchanger.

Question 4

Base on appendices 1 to 4; propose a selection of compressor by justifying your choice of power consumption.

(2 marks)

Question 5

Calculate the mass flow rate and the volume flow rate of vapour passing LP bottle.

(2 marks)

Question 6

To size the LP bottle by considering return or returns pipe at least 0.5 meters of the wall of the bottle, as shown figure below. We will take $k = 0.045$ for the calculation of velocity of separation and base on sizing of vapour section equal to 90% of the cross section of the bottle. Maximum mass of ammonia maintenance in the bottle is evaluated as 650 kg.

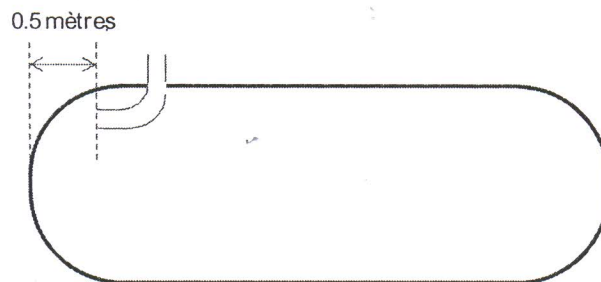


Figure 6.1 Return pipe at least 0.5 meters of the wall of the bottle

(4 marks)

PART C

Question 7

Calculate the discharge temperature which we obtain without oil cooling (we take an isentropic efficiency of 0.7)

(0.5 marks)

Question 8

Explain the role of oil in this application

(0.5 marks)

Question 9

Which place would you position (them) the temperature measurement for controlling oil cooling?

(0.5 marks)

Question 10

Is a system of reheating of oil, necessary? Why?

(0.5 marks)


Question 11

By retaining a manual system of oil recovery, draw the refrigerating diagram of the installation with device of separation of oil cooling and recovery, system of expansion, bottle, condenser, compressor, piping of connections, non-returns valve and oil flow controller positioning in the diagram.

(4 marks)

END OF QUESTION

Appendix 1 Open type screw compressor with R717

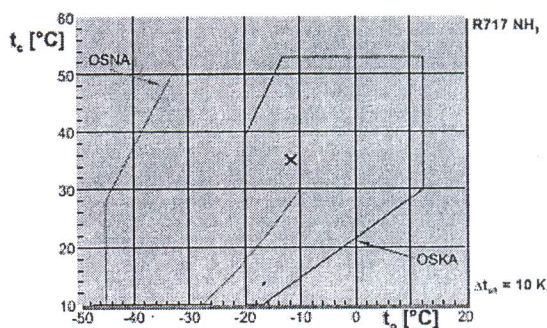
| | |
|--|--|
|  Version 5.1.2 | Appendix 1 Open type screw compressor with R717 4/26/2010 / All data subject to change. |
|--|--|

Compressor Selection: Open Screw Compressors

Input Values

| | |
|-----------------------|-----------------|
| Cooling capacity | 95kW |
| Refrigerant | R717 [NH3] |
| Reference temperature | Dew point temp. |
| Evaporating SST | -12°C |
| Condensing SDT | 35°C |
| Operating mode | Standard |
| Liquid subcooling | 0K |
| Discharge gas temp. | 80°C |
| Suct. gas superheat | 5K |
| Useful superheat | 100% |
| Speed | 2900 /min |
| Capacity Control | 100% |

Application Limits (Standard)



Output


| Compressor model | OSKA7441-K | OSKA7451-K |
|-----------------------|------------|------------|
| Cooling capacity | 92.7 kW | 110.6 kW |
| Cooling capacity * | 92.7 kW | 110.6 kW |
| Evaporator capacity | 92.7 kW | 110.6 kW |
| Power input | 32.2 kW | 33.0 kW |
| Condensing capacity | 106.0 kW | 126.5 kW |
| COP/EER | 2.88 | 3.35 |
| COP/EER * | 2.88 | 3.35 |
| Mass flow LP | 305 kg/h | 364 kg/h |
| Mass flow HP | 305 kg/h | 364 kg/h |
| Operating mode | Standard | Standard |
| Liquid temp. | 35.0 °C | 35.0 °C |
| Oil volume flow | 1.58 m³/h | 1.58 m³/h |
| Oil cooler outlet | 55.3 °C | 57.7 °C |
| Oil cooler load | 18.90 kW | 17.13 kW |
| Necces. driving motor | 37.0 kW | 45.0 kW |
| DG w/o cooling | 167.0 °C | 145.7 °C |

Starting point for motor selection see T. Data/ Notes

Additional cooling/ Limitations (see Limits + T. Data)!

*According to EN12900 (5K suction gas superheat, 0K liquid subcooling)

Appendix 2 Open type screw compressor with R717

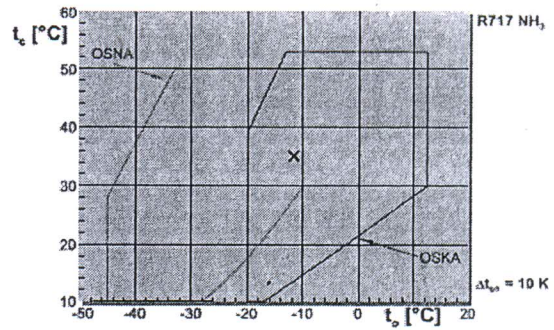
| | |
|--|---|
|  <p>Version 5.1.2</p> | <p>Appendix 2 Open type screw compressor with R717</p> <p>4/26/2010 / All data subject to change.</p> |
|--|---|

Compressor Selection: Open Screw Compressors

Input Values

| | |
|-----------------------|-----------------|
| Cooling capacity | 225kW |
| Refrigerant | R717 [NH3] |
| Reference temperature | Dew point temp. |
| Evaporating SST | -12°C |
| Condensing SDT | 35°C |
| Operating mode | Standard |
| Liquid subcooling | 0K |
| Discharge gas temp. | 80°C |
| Suct. gas superheat | 5K |
| Useful superheat | 100% |
| Speed | 2900 /min |
| Capacity Control | 100% |

Application Limits (Standard)



Output

| Compressor model | OSKA8561-K | OSKA8571-K |
|-----------------------|------------|------------|
| Cooling capacity | 201 kW | 244 kW |
| Cooling capacity * | 201 kW | 244 kW |
| Evaporator capacity | 201 kW | 244 kW |
| Power input | 65.9 kW | 73.8 kW |
| Condensing capacity | 230 kW | 279 kW |
| COP/EER | 3.05 | 3.30 |
| COP/EER * | 3.05 | 3.30 |
| Mass flow LP | 662 kg/h | 801 kg/h |
| Mass flow HP | 662 kg/h | 801 kg/h |
| Operating mode | Standard | Standard |
| Liquid temp. | 35.0 °C | 35.0 °C |
| Oil volume flow | 2.65 m³/h | 2.57 m³/h |
| Oil cooler outlet | 51.1 °C | 48.7 °C |
| Oil cooler load | 37.0 kW | 38.8 kW |
| Necces. driving motor | 90.0 kW | 90.0 kW |
| DG w/o cooling | 158.3 °C | 147.6 °C |

Starting point for motor selection see T. Data/ Notes

Additional cooling/ Limitations (see Limits + T. Data)

*According to EN12900 (5K suction gas superheat, 0K liquid subcooling)

Appendix 3



Grasso Products b.v.

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Comsel - Grasso Sélection de Compresseur

Impression date/heure 09-01-2010 / 16:06
 Version programme 3.8.02 Valide jusqu'au 31/12/2009

PROPRIÉTÉS TECHNIQUES (Package standard)

| | | |
|--------------------------------|------------------|---------------------|
| Screw compressor | 1 x TR-T2240S-28 | |
| Swept volume | 1460,0 | (m ³ /h) |
| Refrigerant | NH3 | |
| Speed | 2940 | (/min) |
| Frequency | 50 | (Hz) |
| Evaporating temperature | -12,0 | (°C) |
| Evaporating pressure | 268,4 | (kPa) |
| Superheat | 5,0 | (K) |
| Useful superheat | 0,0 | (K) |
| Condensing temperature | 35,0 | (°C) |
| Condensing pressure | 1351,3 | (kPa) |
| Liquid subcooling | 0,0 | (K) |
| Pressure ratio | 5,03 | (-) |
| Cooling capacity | 861,4 | (kW) |
| Power Input | 246,7 | (kW) |
| COP = Qo / Pe | 3,49 | (-) |

| Charge partielle [%] * | Pe [kW] | Qo [kW] |
|------------------------|---------|---------|
| 100 | 246,7 | 861,4 |
| 90 | 227,0 | 775,3 |
| 80 | 207,2 | 689,1 |
| 70 | 190,0 | 603,0 |
| 60 | 172,7 | 516,8 |
| 50 | 155,4 | 430,7 |
| 40 | 143,1 | 344,6 |
| 30 | 128,3 | 258,4 |
| 20 | 118,4 | 172,3 |
| 10 | 108,5 | 86,1 |

Partload perc. is not equal to position of control slide perc.
 Partload values are approximate

| | | |
|---------------------------------------|--------|---------|
| Mass flow rate | 2863,0 | (kg/h) |
| Oil cooler load | 120,5 | (kW) |
| Temperature of entering of oil | 50,0 | (°C) |
| Operational flow rate | 49,0 | (l/min) |
| Total flow rate | 128,9 | (l/min) |
| Discharge temperature | 80,0 | (°C) |
| Condensing capacity | 987,6 | (kW) |

Appendix 4



**Grasso
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Comsel - Grasso Sélection de Compresseur

Impression date/heure 09-01-2010 / 00:20
Version programme 3.8.02 Valide jusqu'au 31/12/2009

PROPRIÉTÉS TECHNIQUES (Package standard)

| | | |
|--------------------------------|------------------|--------|
| Screw compressor | 1 x HR-H2655S-28 | |
| Swept volume | 471,0 | (m³/h) |
| Refrigerant | NH3 | |
| Speed | 2940 | (/min) |
| Frequency | 50 | (Hz) |
| Evaporating temperature | -12,0 | (°C) |
| Evaporating pressure | 268,4 | (kPa) |
| Superheat | 5,0 | (K) |
| Useful superheat | 0,0 | (K) |
| Condensing temperature | 35,0 | (°C) |
| Condensing pressure | 1351,3 | (kPa) |
| Liquid subcooling | 0,0 | (K) |
| Pressure ratio | 5,03 | (-) |
| Cooling capacity | 264,9 | (kW) |
| Power input | 79,5 | (kW) |
| COP =Qo / Pe | 3,33 | (-) |

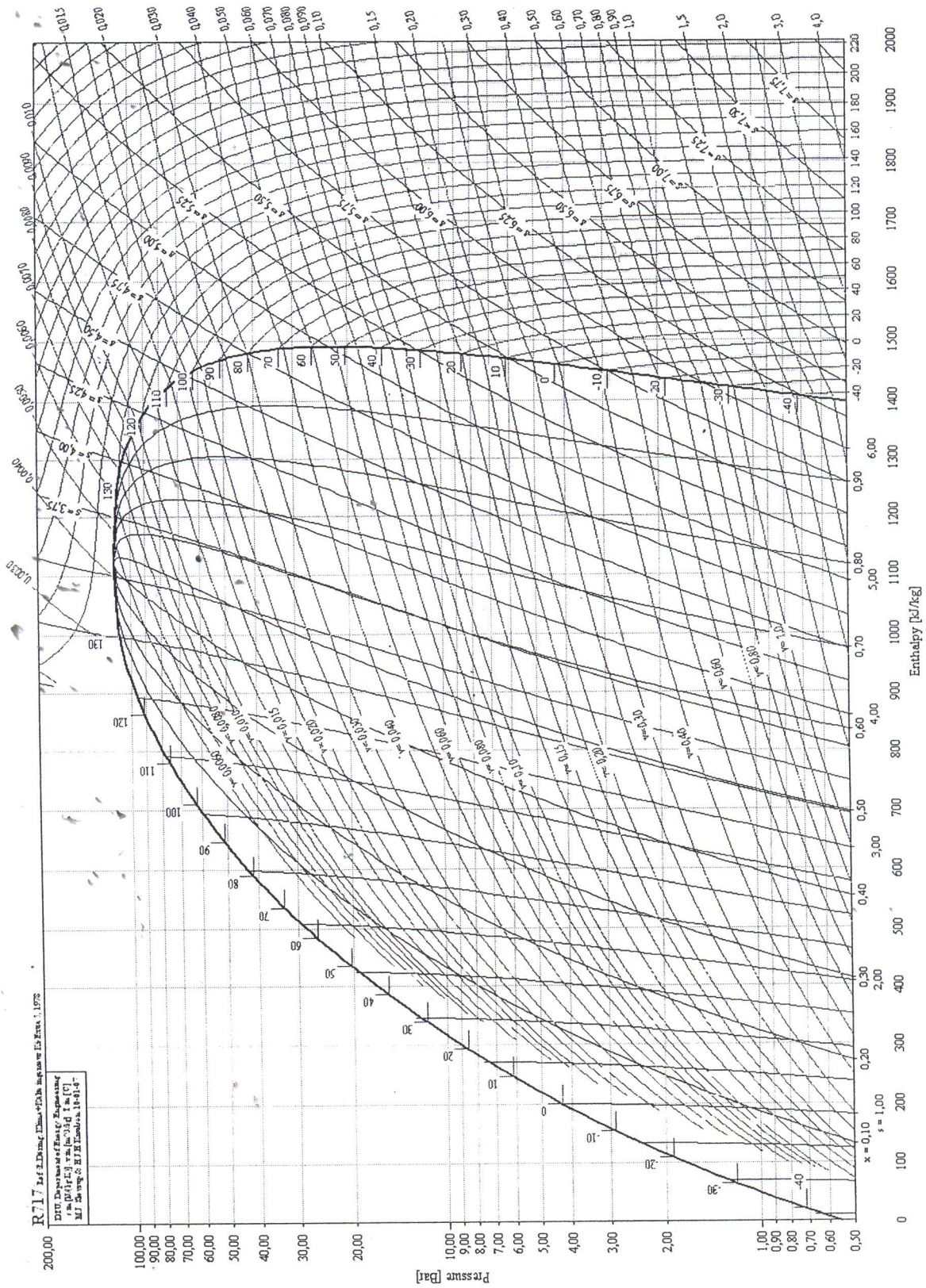
| Charge partielle [%] | Pe [kW] | Qo [kW] |
|----------------------|---------|---------|
| 100 | 79,5 | 264,9 |
| 90 | 73,1 | 238,4 |
| 80 | 66,8 | 211,9 |
| 70 | 61,2 | 185,4 |
| 60 | 55,7 | 158,9 |
| 50 | 50,1 | 132,5 |
| 40 | 46,1 | 106,0 |
| 30 | 41,3 | 79,5 |
| 20 | 38,2 | 53,0 |
| 10 | 35,0 | 26,5 |

Partload perc. is not equal to position of control slide perc.
Partload values are approximate

| | | |
|---------------------------------------|-------|---------|
| Mass flow rate | 880,0 | (kg/h) |
| Oil cooler load | 40,7 | (kW) |
| Temperature of entering of oil | 50,0 | (°C) |
| Operational flow rate | 19,6 | (l/min) |
| Total flow rate | 43,5 | (l/min) |
| Discharge temperature | 80,0 | (°C) |
| Condensing capacity | 303,7 | (kW) |



Appendix 5 PH diagram of R717



Appendix 6 Saturation table of R717

Refrigerant: R717, NH₃, Ammonia, Saturation
 Reference: RDöring, Klima-Kälte ingenieur Ki-Extra 5, 1978

| T °C | P Bar | Vl dm ³ /kg | Vg m ³ /kg | H kJ/kg | Hg kJ/kg | R kJ/kg | S kJ/(kgK) | Sg kJ/(kgK) |
|---------|----------|---------------------------|--------------------------|------------|-------------|------------|---------------|----------------|
| -40 | 0,717 | 1,4491 | 1,55117 | 20,25 | 1407,25 | 1387 | 0,2909 | 6,2398 |
| -38 | 0,797 | 1,4542 | 1,4048 | 29,1 | 1410,38 | 1381,27 | 0,3286 | 6,2026 |
| -36 | 0,885 | 1,4594 | 1,27465 | 37,97 | 1413,46 | 1375,5 | 0,3661 | 6,1662 |
| -34 | 0,98 | 1,4647 | 1,15868 | 46,84 | 1416,51 | 1369,66 | 0,4033 | 6,1305 |
| -32 | 1,083 | 1,4701 | 1,05513 | 55,74 | 1419,5 | 1363,77 | 0,4403 | 6,0956 |
| -30 | 1,195 | 1,4755 | 0,96249 | 64,64 | 1422,46 | 1357,81 | 0,477 | 6,0613 |
| -28 | 1,315 | 1,481 | 0,87945 | 73,57 | 1425,36 | 1351,8 | 0,5135 | 6,0277 |
| -26 | 1,446 | 1,4865 | 0,80488 | 82,5 | 1428,22 | 1345,72 | 0,5497 | 5,9947 |
| -24 | 1,587 | 1,4921 | 0,73779 | 91,45 | 1431,04 | 1339,58 | 0,5857 | 5,9623 |
| -22 | 1,738 | 1,4978 | 0,67733 | 100,42 | 1433,8 | 1333,38 | 0,6214 | 5,9305 |
| -20 | 1,901 | 1,5036 | 0,62274 | 109,4 | 1436,51 | 1327,11 | 0,657 | 5,8994 |
| -18 | 2,076 | 1,5094 | 0,57338 | 118,39 | 1439,17 | 1320,78 | 0,6923 | 5,8687 |
| -16 | 2,263 | 1,5154 | 0,52866 | 127,4 | 1441,78 | 1314,38 | 0,7273 | 5,8386 |
| -14 | 2,464 | 1,5214 | 0,4881 | 136,43 | 1444,34 | 1307,91 | 0,7622 | 5,8091 |
| -12 | 2,679 | 1,5275 | 0,45123 | 145,46 | 1446,84 | 1301,38 | 0,7968 | 5,78 |
| -10 | 2,908 | 1,5336 | 0,41769 | 154,52 | 1449,29 | 1294,77 | 0,8312 | 5,7514 |
| -8 | 3,152 | 1,5399 | 0,38712 | 163,58 | 1451,68 | 1288,09 | 0,8653 | 5,7233 |
| -6 | 3,412 | 1,5463 | 0,35921 | 172,66 | 1454,01 | 1281,35 | 0,8993 | 5,6957 |
| -4 | 3,688 | 1,5527 | 0,33371 | 181,76 | 1456,29 | 1274,53 | 0,9331 | 5,6685 |
| -2 | 3,982 | 1,5593 | 0,31037 | 190,87 | 1458,51 | 1267,63 | 0,9666 | 5,6417 |
| 0 | 4,294 | 1,5659 | 0,28898 | 200 | 1460,66 | 1260,66 | 1 | 5,6153 |
| 2 | 4,625 | 1,5727 | 0,26935 | 209,14 | 1462,76 | 1253,62 | 1,0332 | 5,5893 |
| 4 | 4,975 | 1,5795 | 0,25131 | 218,3 | 1464,8 | 1246,5 | 1,0661 | 5,5637 |
| 6 | 5,345 | 1,5865 | 0,23471 | 227,47 | 1466,77 | 1239,3 | 1,0989 | 5,5384 |
| 8 | 5,737 | 1,5936 | 0,21943 | 236,67 | 1468,68 | 1232,01 | 1,1315 | 5,5135 |
| 10 | 6,15 | 1,6008 | 0,20533 | 245,87 | 1470,52 | 1224,65 | 1,1639 | 5,489 |
| 12 | 6,586 | 1,6081 | 0,19232 | 255,1 | 1472,3 | 1217,21 | 1,1961 | 5,4647 |
| 14 | 7,046 | 1,6155 | 0,18029 | 264,34 | 1474,02 | 1209,67 | 1,2281 | 5,4408 |
| 16 | 7,53 | 1,6231 | 0,16916 | 273,6 | 1475,66 | 1202,06 | 1,26 | 5,4172 |
| 18 | 8,039 | 1,6308 | 0,15885 | 282,89 | 1477,24 | 1194,35 | 1,2917 | 5,3939 |
| 20 | 8,574 | 1,6386 | 0,14929 | 292,19 | 1478,74 | 1186,55 | 1,3232 | 5,3708 |
| 22 | 9,136 | 1,6466 | 0,14041 | 301,51 | 1480,17 | 1178,66 | 1,3546 | 5,3481 |
| 24 | 9,725 | 1,6547 | 0,13216 | 310,86 | 1481,53 | 1170,68 | 1,3859 | 5,3255 |
| 26 | 10,343 | 1,663 | 0,12449 | 320,23 | 1482,82 | 1162,59 | 1,4169 | 5,3033 |
| 28 | 10,991 | 1,6714 | 0,11734 | 329,62 | 1484,03 | 1154,41 | 1,4479 | 5,2812 |
| 30 | 11,669 | 1,68 | 0,11069 | 339,04 | 1485,16 | 1146,12 | 1,4787 | 5,2594 |
| 32 | 12,379 | 1,6888 | 0,10447 | 348,48 | 1486,21 | 1137,73 | 1,5093 | 5,2377 |
| 34 | 13,121 | 1,6978 | 0,09867 | 357,96 | 1487,19 | 1129,23 | 1,5398 | 5,2163 |
| 36 | 13,896 | 1,7069 | 0,09327 | 367,33 | 1488,09 | 1120,75 | 1,5699 | 5,1952 |
| 38 | 14,705 | 1,7162 | 0,0882 | 376,86 | 1488,89 | 1112,03 | 1,6002 | 5,1741 |
| 40 | 15,549 | 1,7257 | 0,08345 | 386,43 | 1489,61 | 1103,19 | 1,6303 | 5,1532 |

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