



**UNIVERSITI KUALA LUMPUR
Malaysia France Institute**

**FINAL EXAMINATION
JANUARY 2010 SESSION**

SUBJECT CODE : FRD 20103
SUBJECT TITLE : THERMODYNAMIC
LEVEL : DIPLOMA
TIME / DURATION : 9.00am – 12.00pm
(3 HOURS)
DATE : 04 MAY 2010

INSTRUCTIONS TO CANDIDATES

1. Please read the instructions given in the question paper CAREFULLY.
2. This question paper is printed on both sides of the paper.
3. Please write your answer on the answer booklet provided.
4. Answer should be written in blue or black ink except for sketching, graphic and illustration.
5. This questions paper consists of TWO (2) sections. Section A and B. Answer ALL questions in Section A. For section B, answer TWO (2) questions only.
6. Answer all questions in English.

THERE ARE 5 PAGES OF QUESTIONS, EXCLUDING THIS PAGE.

SECTION A (Total 60 marks)**INSTRUCTION: Answer ALL questions.****Please use the answer booklet provided.****Question 1**

1) Define the following terms:

- a) Thermodynamic & Heat Transfer
- b) Isothermal process
- c) Isobaric process
- d) Isochoric process

(8 marks)

2). Consider a nuclear power plant that produces 1000MW of power and has a conversion efficiency of 30 percent (that is, for each unit of fuel energy used, the plant produces 0.3 unit of electrical energy). Assuming continuous operation, determine the amount of nuclear fuel consumed by this plant per year? (1 kg of uranium-235 release 6.73×10^10 KJ/kg).

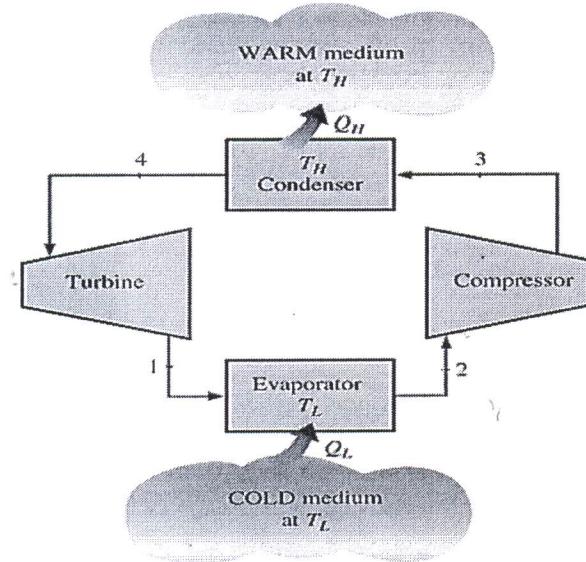
(6 marks)

3) Most of the energy generated in the engine of a car is rejected to the air by the radiator through the circulating water. Should the radiator be analyzed as a closed system or as an open system? Explain.

(6 marks)

Question 2

A refrigerator uses refrigerant-134a as the working fluid and operates on an ideal vapor-compression refrigeration cycle between 0.12 (evaporating pressure) and 0.8 MPa (condensing pressure). An isentropic turbine is used for the expansion/throttling process as shown in Figure 2. No capillary tube is used in this process. The mass flow rate of the refrigerant is 0.05 kg/s. Answer these questions:

**Figure 2 Schematic of a refrigerator**

- (a). Sketch the cycle on a $T - s$ diagram. (5 marks)
- (b). Calculate the rate of heat removal from the refrigerated space (Q_L) in kW. (5 marks)
- (c). Calculate power input to the compressor (W_{in}) in kW. (5 marks)
- (d). Calculate coefficient of performance (COP). (5 marks)

Question 3

Air enters an evaporative cooler at 1 atm, 36°C, and 20 % relative humidity at a rate of 5 m³/min, and it leaves with a relative humidity of 90 % as shown in Figure 3. By assuming that the temperature of the water supplied is equal to the outlet air temperature and the process follows constant wet bulb temperature, by using the psychrometric chart attached:

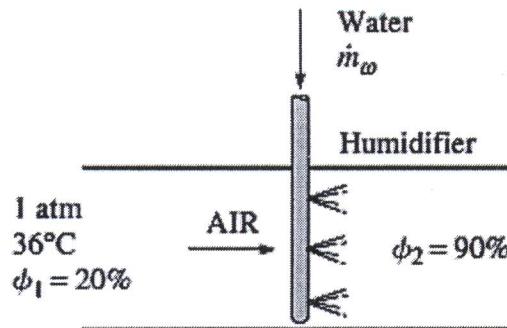
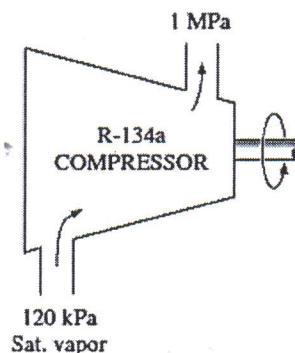


Figure 3 Schematic of a humidifier

- Plot the process on the psychrometric chart attached. (4 marks)
- Determine $T_{\text{wet bulb}}$, ω and v at the inlet to the evaporator. (4 marks)
- Determine $T_{\text{wet bulb}}$ and ω at the outlet of the evaporator. (4 marks)
- Calculate mass flow rate of the dry air in kg/s. (4 marks)
- Calculate mass flow rate of the water supplied(\dot{m}_w) in kg/s. (4 marks)

SECTION B (Total 40 marks)**INSTRUCTION: Answer only TWO questions****Please use the answer booklet provided.****Question 4**

Refrigerant-134a enters an adiabatic compressor as saturated vapor at 120 kPa at a rate of 0.3 m³/min and exits at 1-MPa pressure as shown in Figure 3. If the isentropic efficiency of the compressor is 80 percent, determine:

**Figure 4 A compressor compress R-134a**

- $T_{2\text{ is}}$ and $h_{2\text{ is}}$ at exit of the compressor. (5 marks)
- The actual $h_{2\text{ act}}$ and $T_{2\text{ act}}$ at the exit of the compressor. (5 marks)
- Isentropic and actual work input to the compressor (W_{is} and W_{act}) in kW. (10 marks)

Question 5

a) How does the human body respond to (i) hot weather (ii) cold weather (iii) hot and humid weather? (8 marks)

b) In Figure 5, Air enters a 40-cm-diameter cooling section at 1 atm, 32°C and 30 percent relative humidity at 18 m/s. Heat is removed from the air at a rate of 1200 kJ/min. Determine:

- i) the exit temperature
- ii) the exit relative humidity
- iii) The exit velocity

(12 marks)

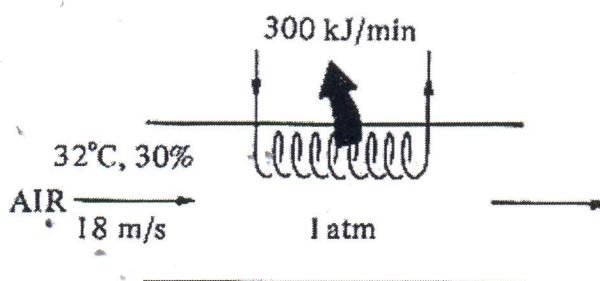


Figure 5

Question 6

Argon gas enters an adiabatic turbine at 800 °C and 1.5 MPa at a mass flow rate of 80 kg/min and exit at 200 kPa. The power output of the turbine is 370 kW and kinetic and potential energies are to be neglected. Argon is assumed to behave as an ideal gas. By taking argon's $C_p = 0.5203 \text{ kJ/kg K}$ and $k = 1.667$, answer these questions.

- a) Calculate the outlet temperature if the compressor is isentropic. (5 marks)
- b) Derive an energy balance equation for the turbine. (5 marks)
- c) Calculate the actual outlet temperature. (5 marks)
- d) Calculate the turbine isentropic efficiency. (5 marks)

END OF QUESTION

APRIL/MAY 2010

CONFIDENTIAL

Appendix

Saturated refrigerant-134a—Temperature table

<i>T</i> °C	<i>P</i> _{sat} kPa	Specific volume, m ³ /kg		Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg · K		
		Sat. liquid, <i>v_f</i>	Sat. vapor, <i>v_g</i>	Sat. liquid, <i>u_f</i>	Evap., <i>u_{fg}</i>	Sat. vapor, <i>u_g</i>	Sat. liquid, <i>h_f</i>	Evap., <i>h_{fg}</i>	Sat. vapor, <i>h_g</i>	Sat. liquid, <i>s_f</i>	Evap., <i>s_{fg}</i>	Sat. vapor, <i>s_g</i>
-40	51.25	0.0007054	0.36081	-0.036	207.40	207.37	0.000	225.86	225.86	0.00000	0.96866	0.96866
-38	56.86	0.0007083	0.32732	2.475	206.04	208.51	2.515	224.61	227.12	0.01072	0.95511	0.96584
-36	62.95	0.0007112	0.29751	4.992	204.67	209.66	5.037	223.35	228.39	0.02138	0.94176	0.96315
-34	69.56	0.0007142	0.27090	7.517	203.29	210.81	7.566	222.09	229.65	0.03199	0.92859	0.96058
-32	76.71	0.0007172	0.24711	10.05	201.91	211.96	10.10	220.81	230.91	0.04253	0.91560	0.95813
-30	84.43	0.0007203	0.22580	12.59	200.52	213.11	12.65	219.52	232.17	0.05301	0.90278	0.95579
-28	92.76	0.0007234	0.20666	15.13	199.12	214.25	15.20	218.22	233.43	0.06344	0.89012	0.95356
-26	101.73	0.0007265	0.18946	17.69	197.72	215.40	17.76	216.92	234.68	0.07382	0.87762	0.95144
-24	111.37	0.0007297	0.17395	20.25	196.30	216.55	20.33	215.59	235.92	0.08414	0.86527	0.94941
-22	121.72	0.0007329	0.16995	22.82	194.88	217.70	22.91	214.26	237.17	0.09441	0.85307	0.94748
-20	132.82	0.0007362	0.14729	25.39	193.45	218.84	25.49	212.91	238.41	0.10463	0.84101	0.94564
-18	144.69	0.0007396	0.13583	27.98	192.01	219.98	28.09	211.55	239.64	0.11481	0.82908	0.94389
-16	157.38	0.0007430	0.12542	30.57	190.56	221.13	30.69	210.18	240.87	0.12493	0.81729	0.94222
-14	170.93	0.0007464	0.11597	33.17	189.09	222.27	33.30	208.79	242.09	0.13501	0.80561	0.94063
-12	185.37	0.0007499	0.10736	35.78	187.62	223.40	35.92	207.38	243.30	0.14504	0.79406	0.93911
-10	200.74	0.0007535	0.099516	38.40	186.14	224.54	38.55	205.96	244.51	0.15504	0.78263	0.93766
-8	217.08	0.0007571	0.092352	41.03	184.64	225.67	41.19	204.52	245.72	0.16498	0.77130	0.93629
-6	234.44	0.0007608	0.085802	43.66	183.13	226.80	43.84	203.07	246.91	0.17489	0.76008	0.93497
-4	252.85	0.0007646	0.079804	46.31	181.61	227.92	46.50	201.60	248.10	0.18476	0.74896	0.93372
-2	272.36	0.0007684	0.074304	48.96	180.08	229.04	49.17	200.11	249.28	0.19459	0.73794	0.93253
0	293.01	0.0007723	0.069255	51.63	178.53	230.16	51.86	198.60	250.45	0.20439	0.72701	0.93139
2	314.84	0.0007763	0.064612	54.30	176.97	231.27	54.55	197.07	251.61	0.21415	0.71616	0.93031
4	337.90	0.0007804	0.060338	56.99	175.39	232.38	57.25	195.51	252.77	0.22387	0.70540	0.92927
6	362.23	0.0007845	0.056398	59.68	173.80	233.48	59.97	193.94	253.91	0.23356	0.69471	0.92828
8	387.88	0.0007887	0.052762	62.39	172.19	234.58	62.69	192.35	255.04	0.24323	0.68410	0.92733
10	414.89	0.0007930	0.049403	65.10	170.56	235.67	65.43	190.73	256.16	0.25286	0.67356	0.92641
12	443.31	0.0007975	0.046295	67.83	168.92	236.75	68.18	189.09	257.27	0.26246	0.66308	0.92554
14	473.19	0.0008020	0.043417	70.57	167.26	237.83	70.95	187.42	258.37	0.27204	0.65266	0.92470
16	504.58	0.0008066	0.040748	73.32	165.58	238.90	73.73	185.73	259.46	0.28159	0.64230	0.92389
18	537.52	0.0008113	0.038271	76.08	163.88	239.96	76.52	184.01	260.53	0.29112	0.63198	0.92310

Saturated refrigerant-134a—Temperature table (Continued)

$T^{\circ}\text{C}$	P_{sat} kPa	Specific volume, m^3/kg			Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg · K		
		Sat. v_f	Sat. v_g	Sat. u_f	Sat. u_{fg}	Sat. u_g	Sat. h_f	Sat. h_{fg}	Sat. h_g	Sat. s_f	Sat. s_{fg}	Sat. s_g	
20	572.07	0.0008161	0.035969	78.86	162.16	241.02	79.32	182.27	261.59	0.30063	0.62172	0.92234	
22	608.27	0.0008210	0.033828	81.64	160.42	242.06	82.14	180.49	262.64	0.31011	0.61149	0.92160	
24	646.18	0.0008261	0.031834	84.44	158.65	243.10	84.98	178.69	263.67	0.31958	0.60130	0.92088	
26	685.84	0.0008313	0.029976	87.26	156.87	244.12	87.83	176.85	264.68	0.32903	0.59115	0.92018	
28	727.31	0.0008366	0.028242	90.09	155.05	245.14	90.69	174.99	265.68	0.33846	0.58102	0.91948	
30	770.64	0.0008421	0.026622	92.93	153.22	246.14	93.58	173.08	266.66	0.34789	0.57091	0.91879	
32	815.89	0.0008478	0.025108	95.79	151.35	247.14	96.48	171.14	267.62	0.35730	0.56082	0.91811	
34	863.11	0.0008536	0.023691	98.66	149.46	248.12	99.40	169.17	268.57	0.36670	0.55074	0.91743	
36	912.35	0.0008595	0.022364	101.55	147.54	249.08	102.33	167.16	269.49	0.37609	0.54066	0.91675	
38	963.68	0.0008657	0.021119	104.45	145.58	250.04	105.29	165.10	270.39	0.38548	0.53058	0.91606	
40	1017.1	0.0008720	0.019952	107.38	143.60	250.97	108.26	163.00	271.27	0.39486	0.52049	0.91536	
42	1072.8	0.0008786	0.018855	110.32	141.58	251.89	111.26	160.86	272.12	0.40425	0.51039	0.91464	
44	1130.7	0.0008854	0.017824	113.28	139.52	252.80	114.28	158.67	272.95	0.41363	0.50027	0.91391	
46	1191.0	0.0008924	0.016853	116.26	137.42	253.68	117.32	156.43	273.75	0.42302	0.49012	0.91315	
48	1253.6	0.0008996	0.015939	119.26	135.29	254.55	120.39	154.14	274.53	0.43242	0.47993	0.91236	
52	1386.2	0.0009150	0.014265	125.33	130.88	256.21	126.59	149.39	275.98	0.45126	0.45941	0.91067	
56	1529.1	0.0009317	0.012771	131.49	126.28	257.77	132.91	144.38	277.30	0.47018	0.43863	0.90880	
60	1682.8	0.0009498	0.011434	137.76	121.46	259.22	139.36	139.10	278.46	0.48920	0.41749	0.90669	
65	1891.0	0.0009750	0.009950	145.77	115.05	260.82	147.62	132.02	279.64	0.51320	0.39039	0.90359	
70	2118.2	0.0010037	0.008642	154.01	108.14	262.15	156.13	124.32	280.46	0.53755	0.36227	0.89982	
75	2365.8	0.0010372	0.007480	162.53	100.60	263.13	164.98	115.85	280.82	0.56241	0.33272	0.89512	
80	2635.3	0.0010772	0.006436	171.40	92.23	263.63	174.24	106.35	280.59	0.58800	0.30111	0.88912	
85	2928.2	0.0011270	0.005486	180.77	82.67	263.44	184.07	95.44	279.51	0.61473	0.26644	0.88117	
90	3246.9	0.0011932	0.004599	190.89	71.29	262.18	194.76	82.35	277.11	0.64336	0.22674	0.87010	
95	3594.1	0.0012933	0.003726	202.40	56.47	258.87	207.05	65.21	272.26	0.67578	0.17711	0.85289	
100	3975.1	0.0015269	0.002630	218.72	29.19	247.91	224.79	33.58	258.37	0.72217	0.08999	0.81215	

Saturated refrigerant-134a—Pressure table

Press., P kPa	Sat. temp., T_{sat} °C	Specific volume, m³/kg			Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg · K		
		Sat. liquid, v_f	Sat. vapor, v_g	Sat. liquid, u_f	Sat. Evap., u_{fg}	Sat. vapor, u_g	Sat. liquid, h_f	Sat. Evap., h_{fg}	Sat. vapor, h_g	Sat. liquid, s_f	Sat. Evap., s_{fg}	Sat. vapor, s_g	
60	-36.95	0.0007098	0.31121	3.798	205.32	209.12	3.841	223.95	227.79	0.01634	0.94807	0.96441	
70	-33.87	0.0007144	0.26929	7.680	203.20	210.88	7.730	222.00	229.73	0.03267	0.92775	0.96042	
80	-31.13	0.0007185	0.23753	11.15	201.30	212.46	11.21	220.25	231.46	0.04711	0.90999	0.95710	
90	-28.65	0.0007223	0.21263	14.31	199.57	213.88	14.37	218.65	233.02	0.06008	0.89419	0.95427	
100	-26.37	0.0007259	0.19254	17.21	197.98	215.19	17.28	217.16	234.44	0.07188	0.87995	0.95183	
120	-22.32	0.0007324	0.16212	22.40	195.11	217.51	22.49	214.48	236.97	0.09275	0.85503	0.94779	
140	-18.77	0.0007383	0.14014	26.98	192.57	219.54	27.08	212.08	239.16	0.11087	0.83368	0.94456	
160	-15.60	0.0007437	0.12348	31.09	190.27	221.35	31.21	209.90	241.11	0.12693	0.81496	0.94190	
180	-12.73	0.0007487	0.11041	34.83	188.16	222.99	34.97	207.90	242.86	0.14139	0.79826	0.93965	
200	-10.09	0.0007533	0.099867	38.28	186.21	224.48	38.43	206.03	244.46	0.15457	0.78316	0.93773	
240	-5.38	0.0007620	0.083897	44.48	182.67	227.14	44.66	202.62	247.28	0.17794	0.75664	0.93458	
280	-1.25	0.0007699	0.072352	49.97	179.50	229.46	50.18	199.54	249.72	0.19829	0.73381	0.93210	
320	2.46	0.0007772	0.063604	54.92	176.61	231.52	55.16	196.71	251.88	0.21637	0.71369	0.93006	
360	5.82	0.0007841	0.056738	59.44	173.94	233.38	59.72	194.08	253.81	0.23270	0.69566	0.92836	
400	8.91	0.0007907	0.051201	63.62	171.45	235.07	63.94	191.62	255.55	0.24761	0.67929	0.92691	
450	12.46	0.0007985	0.045619	68.45	168.54	237.00	68.81	188.71	257.53	0.26465	0.66069	0.92535	
500	15.71	0.0008059	0.041118	72.93	165.82	238.75	73.33	185.98	259.30	0.28023	0.64377	0.92400	
550	18.73	0.0008130	0.037408	77.10	163.25	240.35	77.54	183.38	260.92	0.29461	0.62821	0.92282	
600	21.55	0.0008199	0.034295	81.02	160.81	241.83	81.51	180.90	262.40	0.30799	0.61378	0.92177	
650	24.20	0.0008266	0.031646	84.72	158.48	243.20	85.26	178.51	263.77	0.32051	0.60030	0.92081	
700	26.69	0.0008331	0.029361	88.24	156.24	244.48	88.82	176.21	265.03	0.33230	0.58763	0.91994	
750	29.06	0.0008395	0.027371	91.59	154.08	245.67	92.22	173.98	266.20	0.34345	0.57567	0.91912	
800	31.31	0.0008458	0.025621	94.79	152.00	246.79	95.47	171.82	267.29	0.35404	0.56431	0.91835	
850	33.45	0.0008520	0.024069	97.87	149.98	247.85	98.60	169.71	268.31	0.36413	0.55349	0.91762	
900	35.51	0.0008580	0.022683	100.83	148.01	248.85	101.61	167.66	269.26	0.37377	0.54315	0.91692	
950	37.48	0.0008641	0.021438	103.69	146.10	249.79	104.51	165.64	270.15	0.38301	0.53323	0.91624	
1000	39.37	0.0008700	0.020313	106.45	144.23	250.68	107.32	163.67	270.99	0.39189	0.52368	0.91558	
1200	46.29	0.0008934	0.016715	116.70	137.11	253.81	117.77	156.10	273.87	0.42441	0.48863	0.91303	
1400	52.40	0.0009166	0.014107	125.94	130.43	256.37	127.22	148.90	276.12	0.45315	0.45734	0.91050	
1600	57.88	0.0009400	0.012123	134.43	124.04	258.47	135.93	141.93	277.86	0.47911	0.42873	0.90784	
1800	62.87	0.0009639	0.010559	142.33	117.83	260.17	144.07	135.11	279.17	0.50294	0.40204	0.90498	
2000	67.45	0.0009886	0.009288	149.78	111.73	261.51	151.76	128.33	280.09	0.52509	0.37675	0.90184	
2500	77.54	0.0010566	0.006936	166.99	96.47	263.45	169.63	111.16	280.79	0.57531	0.31695	0.89226	
3000	86.16	0.0011406	0.005275	183.04	80.22	263.26	186.46	92.63	279.09	0.62118	0.25776	0.87894	

Superheated refrigerant-134a

T °C	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K
<i>P = 0.06 MPa (T_{sat} = -36.95°C)</i>					<i>P = 0.10 MPa (T_{sat} = -26.37°C)</i>					<i>P = 0.14 MPa (T_{sat} = -18.77°C)</i>		
Sat.	0.31121	209.12	227.79	0.9644	0.19254	215.19	234.44	0.9518	0.14014	219.54	239.16	0.9446
-20	0.33608	220.60	240.76	1.0174	0.19841	219.66	239.50	0.9721	0.14605	225.91	246.36	0.9724
-10	0.35048	227.55	248.58	1.0477	0.20743	226.75	247.49	1.0030	0.15263	233.23	254.60	1.0031
0	0.36476	234.66	256.54	1.0774	0.21630	233.95	255.58	1.0332	0.15908	240.66	262.93	1.0331
10	0.37893	241.92	264.66	1.1066	0.22506	241.30	263.81	1.0628	0.16544	248.22	271.38	1.0624
20	0.39302	249.35	272.94	1.1353	0.23373	248.79	272.17	1.0918	0.17172	255.93	279.97	1.0912
30	0.40705	256.95	281.37	1.1636	0.24233	256.44	280.68	1.1203	0.17794	263.79	288.70	1.1195
40	0.42102	264.71	289.97	1.1915	0.25088	264.25	289.34	1.1484	0.18412	271.79	297.57	1.1474
50	0.43495	272.64	298.74	1.2191	0.25937	272.22	298.16	1.1762	0.19025	279.96	306.59	1.1749
60	0.44883	280.73	307.66	1.2463	0.26783	280.35	307.13	1.2035	0.19635	288.28	315.77	1.2020
70	0.46269	288.99	316.75	1.2732	0.27626	288.64	316.26	1.2305	0.20242	296.75	325.09	1.2288
80	0.47651	297.41	326.00	1.2997	0.28465	297.08	325.55	1.2572	0.20847	305.38	334.57	1.2553
90	0.49032	306.00	335.42	1.3260	0.29303	305.69	334.99	1.2836	0.21449	314.17	344.20	1.2814
100	0.50410	314.74	344.99	1.3520	0.30138	314.46	344.60	1.3096				
<i>P = 0.18 MPa (T_{sat} = -12.73°C)</i>					<i>P = 0.20 MPa (T_{sat} = -10.09°C)</i>					<i>P = 0.24 MPa (T_{sat} = -5.38°C)</i>		
Sat.	0.11041	222.99	242.86	0.9397	0.09987	224.48	244.46	0.9377	0.08390	227.14	247.28	0.9346
-10	0.11189	225.02	245.16	0.9484	0.09991	224.55	244.54	0.9380	0.08617	231.29	251.97	0.9519
0	0.11722	232.48	253.58	0.9798	0.10481	232.09	253.05	0.9698	0.09026	238.98	260.65	0.9831
10	0.12240	240.00	262.04	1.0102	0.10955	239.67	261.58	1.0004	0.09423	246.74	269.36	1.0134
20	0.12748	247.64	270.59	1.0399	0.11418	247.35	270.18	1.0303	0.09812	254.61	278.16	1.0429
30	0.13248	255.41	279.25	1.0690	0.11874	255.14	278.89	1.0595	0.10193	262.59	287.06	1.0718
40	0.13741	263.31	288.05	1.0975	0.12322	263.08	287.72	1.0882	0.10570	270.71	296.08	1.1001
50	0.14230	271.36	296.98	1.1256	0.12766	271.15	296.68	1.1163	0.10942	278.97	305.23	1.1280
60	0.14715	279.56	306.05	1.1532	0.13206	279.37	305.78	1.1441	0.11310	287.36	314.51	1.1554
70	0.15196	287.91	315.27	1.1805	0.13641	287.73	315.01	1.1714	0.11675	295.91	323.93	1.1825
80	0.15673	296.42	324.63	1.2074	0.14074	296.25	324.40	1.1983	0.12038	304.60	333.49	1.2092
90	0.16149	305.07	334.14	1.2339	0.14504	304.92	333.93	1.2249	0.12398	313.44	343.20	1.2356
100	0.16622	313.88	343.80	1.2602	0.14933	313.74	343.60	1.2512				
<i>P = 0.28 MPa (T_{sat} = -1.25°C)</i>					<i>P = 0.32 MPa (T_{sat} = 2.46°C)</i>					<i>P = 0.40 MPa (T_{sat} = 8.91°C)</i>		
Sat.	0.07235	229.46	249.72	0.9321	0.06360	231.52	251.88	0.9301	0.051201	235.07	255.55	0.9269
0	0.07282	230.44	250.83	0.9362	0.06609	237.54	258.69	0.9544	0.051506	235.97	256.58	0.9305
10	0.07646	238.27	259.68	0.9680	0.06925	245.50	267.66	0.9856	0.054213	244.18	265.86	0.9628
20	0.07997	246.13	268.52	0.9987	0.07231	253.50	276.65	1.0157	0.056796	252.36	275.07	0.9937
30	0.08338	254.06	277.41	1.0285	0.07530	261.60	285.70	1.0451	0.059292	260.58	284.30	1.0236
40	0.08672	262.10	286.38	1.0576	0.07823	269.82	294.85	1.0739	0.061724	268.90	293.59	1.0528
50	0.09000	270.27	295.47	1.0862	0.08111	278.15	304.11	1.1021	0.064104	277.32	302.96	1.0814
60	0.09324	278.56	304.67	1.1142	0.08395	286.62	313.48	1.1298	0.066443	285.86	312.44	1.1094
70	0.09644	286.99	314.00	1.1418	0.08675	295.22	322.98	1.1571	0.068747	294.53	322.02	1.1369
80	0.09961	295.57	323.46	1.1690	0.08953	303.97	332.62	1.1840	0.071023	303.32	331.73	1.1640
90	0.10275	304.29	333.06	1.1958	0.09229	312.86	342.39	1.2105	0.073274	312.26	341.57	1.1907
100	0.10587	313.15	342.80	1.2222	0.09503	321.89	352.30	1.2367	0.075504	321.33	351.53	1.2171
110	0.10897	322.16	352.68	1.2483	0.09775	331.07	362.35	1.2626	0.077717	330.55	361.63	1.2431
120	0.11205	331.32	362.70	1.2742	0.10045	340.39	372.54	1.2882	0.079913	339.90	371.87	1.2688
130	0.11512	340.63	372.87	1.2997	0.10314	349.86	382.87	1.3135	0.082096	349.41	382.24	1.2942

Superheated refrigerant-134a (Continued)

T °C	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K	v m ³ /kg	u kJ/kg	h kJ/kg	s kJ/kg · K
<i>P = 0.50 MPa (T_{sat} = 15.71°C)</i>					<i>P = 0.60 MPa (T_{sat} = 21.55°C)</i>					<i>P = 0.70 MPa (T_{sat} = 26.69°C)</i>		
Sat.	0.041118	238.75	259.30	0.9240	0.034295	241.83	262.40	0.9218	0.029361	244.48	265.03	0.9199
20	0.042115	242.40	263.46	0.9383	0.035984	249.22	270.81	0.9499	0.029966	247.48	268.45	0.9313
30	0.044338	250.84	273.01	0.9703	0.037865	257.86	280.58	0.9816	0.031696	256.39	278.57	0.9641
40	0.046456	259.26	282.48	1.0011	0.039659	266.48	290.28	1.0121	0.033322	265.20	288.53	0.9954
50	0.048499	267.72	291.96	1.0309	0.041389	275.15	299.98	1.0417	0.034875	274.01	298.42	1.0256
60	0.050485	276.25	301.50	1.0599	0.043069	283.89	309.73	1.0705	0.036373	282.87	308.33	1.0549
70	0.052427	284.89	311.10	1.0883	0.044710	292.73	319.55	1.0987	0.037829	291.80	318.28	1.0835
80	0.054331	293.64	320.80	1.1162	0.046318	301.67	329.46	1.1264	0.039250	300.82	328.29	1.1114
90	0.056205	302.51	330.61	1.1436	0.047900	310.73	339.47	1.1536	0.040642	309.95	338.40	1.1389
100	0.058053	311.50	340.53	1.1705	0.049458	319.91	349.59	1.1803	0.042010	319.19	348.60	1.1658
110	0.059880	320.63	350.57	1.1971	0.050997	329.23	359.82	1.2067	0.043358	328.55	358.90	1.1924
120	0.061687	329.89	360.73	1.2233	0.052519	338.67	370.18	1.2327	0.044688	338.04	369.32	1.2186
130	0.063479	339.29	371.03	1.2491	0.054027	348.25	380.66	1.2584	0.046004	347.66	379.86	1.2444
140	0.065256	348.83	381.46	1.2747	0.055522	357.96	391.27	1.2838	0.047306	357.41	390.52	1.2699
150	0.067021	358.51	392.02	1.2999	0.057006	367.81	402.01	1.3088	0.048597	367.29	401.31	1.2951
160	0.068775	368.33	402.72	1.3249	<i>P = 0.80 MPa (T_{sat} = 31.31°C)</i>					<i>P = 1.00 MPa (T_{sat} = 39.37°C)</i>		
Sat.	0.025621	246.79	267.29	0.9183	0.022683	248.85	269.26	0.9169	0.020313	250.68	270.99	0.9156
40	0.027035	254.82	276.45	0.9480	0.023375	253.13	274.17	0.9327	0.020406	251.30	271.71	0.9179
50	0.028547	263.86	286.69	0.9802	0.024809	262.44	284.77	0.9660	0.021796	260.94	282.74	0.9525
60	0.029973	272.83	296.81	1.0110	0.026146	271.60	295.13	0.9976	0.023068	270.32	293.38	0.9850
70	0.031340	281.81	306.88	1.0408	0.027413	280.72	305.39	1.0280	0.024261	279.59	303.85	1.0160
80	0.032659	290.84	316.97	1.0698	0.028630	289.86	315.63	1.0574	0.025398	288.86	314.25	1.0458
90	0.033941	299.95	327.10	1.0981	0.029806	299.06	325.89	1.0860	0.026492	298.15	324.64	1.0748
100	0.035193	309.15	337.30	1.1258	0.030951	308.34	336.19	1.1140	0.027552	307.51	335.06	1.1031
110	0.036420	318.45	347.59	1.1530	0.032068	317.70	346.56	1.1414	0.028584	316.94	345.53	1.1308
120	0.037625	327.87	357.97	1.1798	0.033164	327.18	357.02	1.1684	0.029592	326.47	356.06	1.1580
130	0.038813	337.40	368.45	1.2061	0.034241	336.76	367.58	1.1949	0.030581	336.11	366.69	1.1846
140	0.039985	347.06	379.05	1.2321	0.035302	346.46	378.23	1.2210	0.031554	345.85	377.40	1.2109
150	0.041143	356.85	389.76	1.2577	0.036349	356.28	389.00	1.2467	0.032512	355.71	388.22	1.2368
160	0.042290	366.76	400.59	1.2830	0.037384	366.23	399.88	1.2721	0.033457	365.70	399.15	1.2623
170	0.043427	376.81	411.55	1.3080	0.038408	376.31	410.88	1.2972	0.034392	375.81	410.20	1.2875
180	0.044554	386.99	422.64	1.3327	0.039423	386.52	422.00	1.3221	0.035317	386.04	421.36	1.3124
<i>P = 1.20 MPa (T_{sat} = 46.29°C)</i>					<i>P = 1.40 MPa (T_{sat} = 52.40°C)</i>					<i>P = 1.60 MPa (T_{sat} = 57.88°C)</i>		
Sat.	0.016715	253.81	273.87	0.9130	0.014107	256.37	276.12	0.9105	0.012123	258.47	277.86	0.9078
50	0.017201	257.63	278.27	0.9267	0.015005	264.46	285.47	0.9389	0.012372	260.89	280.69	0.9163
60	0.018404	267.56	289.64	0.9614	0.016060	274.62	297.10	0.9733	0.013430	271.76	293.25	0.9535
70	0.019502	277.21	300.61	0.9938	0.017023	284.51	308.34	1.0056	0.014362	282.09	305.07	0.9875
80	0.020529	286.75	311.39	1.0248	0.017923	294.28	319.37	1.0364	0.015215	292.17	316.52	1.0194
90	0.021506	296.26	322.07	1.0546	0.018778	304.01	330.30	1.0661	0.016014	302.14	327.76	1.0500
100	0.022442	305.80	332.73	1.0836	0.019597	313.76	341.19	1.0949	0.016773	312.07	338.91	1.0795
110	0.023348	315.38	343.40	1.1118	0.020388	323.55	352.09	1.1230	0.017500	322.02	350.02	1.1081
120	0.024228	325.03	354.11	1.1394	0.021155	333.41	363.02	1.1504	0.018201	332.00	361.12	1.1360
130	0.025086	334.77	364.88	1.1664	0.021904	343.34	374.01	1.1773	0.018882	342.05	372.26	1.1632
140	0.025927	344.61	375.72	1.1930	0.022636	353.37	385.07	1.2038	0.019545	352.17	383.44	1.1900
150	0.026753	354.56	386.66	1.2192	0.023355	363.51	396.20	1.2298	0.020194	362.38	394.69	1.2163
160	0.027566	364.61	397.69	1.2449	0.024061	373.75	407.43	1.2554	0.020830	372.69	406.02	1.2421
170	0.028367	374.78	408.82	1.2703	0.024757	384.10	418.76	1.2807	0.021456	383.11	417.44	1.2676

Ideal-gas properties of air

<i>T</i> K	<i>h</i> kJ/kg	<i>P_r</i>	<i>u</i> kJ/kg	<i>v_r</i>	<i>s^o</i> kJ/kg · K	<i>T</i> K	<i>h</i> kJ/kg	<i>P_r</i>	<i>u</i> kJ/kg	<i>v_r</i>	<i>s^o</i> kJ/kg · K
200	199.97	0.3363	142.56	1707.0	1.29559	580	586.04	14.38	419.55	115.7	2.37348
210	209.97	0.3987	149.69	1512.0	1.34444	590	596.52	15.31	427.15	110.6	2.39140
220	219.97	0.4690	156.82	1346.0	1.39105	600	607.02	16.28	434.78	105.8	2.40902
230	230.02	0.5477	164.00	1205.0	1.43557	610	617.53	17.30	442.42	101.2	2.42644
240	240.02	0.6355	171.13	1084.0	1.47824	620	628.07	18.36	450.09	96.92	2.44356
250	250.05	0.7329	178.28	979.0	1.51917	630	638.63	19.84	457.78	92.84	2.46048
260	260.09	0.8405	185.45	887.8	1.55848	640	649.22	20.64	465.50	88.99	2.47716
270	270.11	0.9590	192.60	808.0	1.59634	650	659.84	21.86	473.25	85.34	2.49364
280	280.13	1.0889	199.75	738.0	1.63279	660	670.47	23.13	481.01	81.89	2.50985
285	285.14	1.1584	203.33	706.1	1.65055	670	681.14	24.46	488.81	78.61	2.52589
290	290.16	1.2311	206.91	676.1	1.66802	680	691.82	25.85	496.62	75.50	2.54175
295	295.17	1.3068	210.49	647.9	1.68515	690	702.52	27.29	504.45	72.56	2.55731
298	298.18	1.3543	212.64	631.9	1.69528	700	713.27	28.80	512.33	69.76	2.57277
300	300.19	1.3860	214.07	621.2	1.70203	710	724.04	30.38	520.23	67.07	2.58810
305	305.22	1.4686	217.67	596.0	1.71865	720	734.82	32.02	528.14	64.53	2.60319
310	310.24	1.5546	221.25	572.3	1.73498	730	745.62	33.72	536.07	62.13	2.61803
315	315.27	1.6442	224.85	549.8	1.75106	740	756.44	35.50	544.02	59.82	2.63280
320	320.29	1.7375	228.42	528.6	1.76690	750	767.29	37.35	551.99	57.63	2.64737
325	325.31	1.8345	232.02	508.4	1.78249	760	778.18	39.27	560.01	55.54	2.66176
330	330.34	1.9352	235.61	489.4	1.79783	780	800.03	43.35	576.12	51.64	2.69013
340	340.42	2.149	242.82	454.1	1.82790	800	821.95	47.75	592.30	48.08	2.71787
350	350.49	2.379	250.02	422.2	1.85708	820	843.98	52.59	608.59	44.84	2.74504
360	360.58	2.626	257.24	393.4	1.88543	840	866.08	57.60	624.95	41.85	2.77170
370	370.67	2.892	264.46	367.2	1.91313	860	888.27	63.09	641.40	39.12	2.79783
380	380.77	3.176	271.69	343.4	1.94001	880	910.56	68.98	657.95	36.61	2.82344
390	390.88	3.481	278.93	321.5	1.96633	900	932.93	75.29	674.58	34.31	2.84856
400	400.98	3.806	286.16	301.6	1.99194	920	955.38	82.05	691.28	32.18	2.87324
410	411.12	4.153	293.43	283.3	2.01699	940	977.92	89.28	708.08	30.22	2.89748
420	421.26	4.522	300.69	266.6	2.04142	960	1000.55	97.00	725.02	28.40	2.92128
430	431.43	4.915	307.99	251.1	2.06533	980	1023.25	105.2	741.98	26.73	2.94468
440	441.61	5.332	315.30	236.8	2.08870	1000	1046.04	114.0	758.94	25.17	2.96770
450	451.80	5.775	322.62	223.6	2.11161	1020	1068.89	123.4	776.10	23.72	2.99034
460	462.02	6.245	329.97	211.4	2.13407	1040	1091.85	133.3	793.36	23.29	3.01260
470	472.24	6.742	337.32	200.1	2.15604	1060	1114.86	143.9	810.62	21.14	3.03449
480	482.49	7.268	344.70	189.5	2.17760	1080	1137.89	155.2	827.88	19.98	3.05608
490	492.74	7.824	352.08	179.7	2.19876	1100	1161.07	167.1	845.33	18.896	3.07732
500	503.02	8.411	359.49	170.6	2.21952	1120	1184.28	179.7	862.79	17.886	3.09825
510	513.32	9.031	366.92	162.1	2.23993	1140	1207.57	193.1	880.35	16.946	3.11883
520	523.63	9.684	374.36	154.1	2.25997	1160	1230.92	207.2	897.91	16.064	3.13916
530	533.98	10.37	381.84	146.7	2.27967	1180	1254.34	222.2	915.57	15.241	3.15916
540	544.35	11.10	389.34	139.7	2.29906	1200	1277.79	238.0	933.33	14.470	3.17888
550	555.74	11.86	396.86	133.1	2.31809	1220	1301.31	254.7	951.09	13.747	3.19834
560	565.17	12.66	404.42	127.0	2.33685	1240	1324.93	272.3	968.95	13.069	3.21751
570	575.59	13.50	411.97	121.2	2.35531						

Ideal-gas properties of air (Concluded)

T K	<i>h</i> kJ/kg	<i>P_r</i>	<i>u</i> kJ/kg	<i>v_r</i>	<i>s^o</i> kJ/kg · K	T K	<i>h</i> kJ/kg	<i>P_r</i>	<i>u</i> kJ/kg	<i>v_r</i>	<i>s^o</i> kJ/kg · K
1260	1348.55	290.8	986.90	12.435	3.23638	1600	1757.57	791.2	1298.30	5.804	3.5236
1280	1372.24	310.4	1004.76	11.835	3.25510	1620	1782.00	834.1	1316.96	5.574	3.5387
1300	1395.97	330.9	1022.82	11.275	3.27345	1640	1806.46	878.9	1335.72	5.355	3.5538
1320	1419.76	352.5	1040.88	10.747	3.29160	1660	1830.96	925.6	1354.48	5.147	3.5686
1340	1443.60	375.3	1058.94	10.247	3.30959	1680	1855.50	974.2	1373.24	4.949	3.5833
1360	1467.49	399.1	1077.10	9.780	3.32724	1700	1880.1	1025	1392.7	4.761	3.5979
1380	1491.44	424.2	1095.26	9.337	3.34474	1750	1941.6	1161	1439.8	4.328	3.6336
1400	1515.42	450.5	1113.52	8.919	3.36200	1800	2003.3	1310	1487.2	3.994	3.6684
1420	1539.44	478.0	1131.77	8.526	3.37901	1850	2065.3	1475	1534.9	3.601	3.7023
1440	1563.51	506.9	1150.13	8.153	3.39586	1900	2127.4	1655	1582.6	3.295	3.7354
1460	1587.63	537.1	1168.49	7.801	3.41247	1950	2189.7	1852	1630.6	3.022	3.7677
1480	1611.79	568.8	1186.95	7.468	3.42892	2000	2252.1	2068	1678.7	2.776	3.7994
1500	1635.97	601.9	1205.41	7.152	3.44516	2050	2314.6	2303	1726.8	2.555	3.8303
1520	1660.23	636.5	1223.87	6.854	3.46120	2100	2377.7	2559	1775.3	2.356	3.8605
1540	1684.51	672.8	1242.43	6.569	3.47712	2150	2440.3	2837	1823.8	2.175	3.8901
1560	1708.82	710.5	1260.99	6.301	3.49276	2200	2503.2	3138	1872.4	2.012	3.9191
1580	1733.17	750.0	1279.65	6.046	3.50829	2250	2566.4	3464	1921.3	1.864	3.9474

Useful Formula

(1) Work Relations

$$W_b = \int pdV$$

$$W_e = VI\Delta t$$

$$W_{\text{spring}} = \frac{k_s}{2}(x_2^2 - x_1^2)$$

$$W_{\text{rot}} = 2\pi n\tau$$

$$W_{\text{cv}} = -\int_1^2 vdp + (V_1^2 - V_2^2)/2 + g(z_1 - z_2)$$

(2) First Law Relations and Mass Conservation

$$Q - W = \Delta U + \Delta KE + \Delta PE \quad \frac{dE}{dt} = \dot{Q} - \dot{W}$$

$$\dot{Q}_{\text{cv}} - \dot{W}_{\text{cv}} - \sum_e \dot{m}_e (h + V^2/2 + gz)_e + \sum_i \dot{m}_i (h + V^2/2 + gz)_i = \frac{dE}{dt} \Big|_{\text{cv}}$$

$$\dot{m} = \rho VA \quad \sum_e \dot{m}_e = \sum_i \dot{m}_i$$

(3) Second Law Relations

$$\Delta S = \int_1^2 \left[\frac{\delta Q}{T} \right]_b + S_{\text{gen}}$$

$$\Delta S = \int_1^2 \left[\frac{\delta q}{T} \right]_{\text{int rev}}$$

$$\frac{dS}{dt} = \sum_j \frac{\dot{Q}_j}{T_j} + \dot{S}_{\text{gen}}$$

$$-\sum_e \dot{m}_e s_e + \sum_i \dot{m}_i s_i + \sum_j \frac{\dot{Q}_j}{T_j} + \dot{S}_{\text{gen, cv}} = \frac{dS_{\text{cv}}}{dt}$$

(4) Pressure, Temperature and Energy Relations

$$\begin{array}{lll}
 p_{\text{abs}} = p_{\text{atm}} \pm p_{\text{gage}} & p - p_{\text{atm}} = \rho g L \\
 pV = n\bar{R}T & pV = mRT & R = \bar{R}/M \quad pV = ZRT \\
 p_R = p/p_c & T_R = T/T_c & v_R = v p_c / RT_c \quad k = C_p/C_v \\
 x = m_g / (m_f + m_g) & y = (1-x)y_f + xy_g = y_f + xy_{fg} & y_{fg} = y_g - y_f \\
 h = u + pv & \Delta u = \int c_v dT & \Delta h = \int c_p dT \quad c_p - c_v = R \\
 \Delta u = \int cdT & \Delta h = \Delta u + v\Delta p & h(T, p) - h_f(T) = v_f(T)[p - p_{\text{sat}}(T)]
 \end{array}$$

(5) Entropy Relations (and isentropic processes)

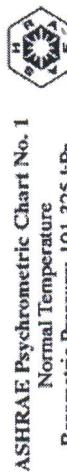
$$\begin{array}{lll}
 Tds = du + pdv & Tds = dh - vdp \\
 ds = c_v \frac{dT}{T} + R \frac{dv}{v} & ds = c_p \frac{dT}{T} - R \frac{dp}{p} \\
 \Delta s = s_2^o - s_1^o - R \ln(p_2 / p_1) & \Delta s = c \ln(T_2 / T_1) \\
 T_2 / T_1 = (p_2 / p_1)^{(k-1)/k} = (v_1 / v_2)^{k-1} \quad (p_2 / p_1)_s = p_{r2} / p_{r1} \quad (v_2 / v_1)_s = v_{r2} / v_{r1}
 \end{array}$$

(6) Device Efficiencies and Cycle Analyses

$$\begin{array}{lll}
 \eta_{\text{turbine}} = w_{\text{act}} / w_{\text{isen}} & \eta_{\text{comp}} = \eta_{\text{pump}} = w_{\text{isen}} / w_{\text{act}} & \eta_{\text{nozzle}} = V_{2,\text{act}}^2 / V_{2,\text{isen}}^2 \\
 \eta_{\text{th}} = \frac{W_{\text{net,out}}}{Q_H} & \text{COP}_R = \frac{Q_L}{W_{\text{net,in}}} & \text{COP}_{HP} = \frac{Q_H}{W_{\text{net,in}}} \\
 \eta_{\text{th,rev}} = 1 - \frac{T_L}{T_H} & \text{COP}_{R,\text{rev}} = \frac{T_L}{T_H - T_L} & \text{COP}_{HP,\text{rev}} = \frac{T_H}{T_H - T_L} \quad \frac{T_C}{T_H} = \left(\frac{Q_C}{Q_H} \right)_{\text{rev}}
 \end{array}$$

APRIL/MAY 2010

CONFIDENTIAL



©1992 American Society of Heating,
Refrigerating and Air-Conditioning Engineers, Inc.

Sea Level

